

# Globular Structures of a Helix-Coil Copolymer: Self-Consistent Treatment.

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A self-consistent field theory was developed in the grand-canonical ensemble formulation to study transitions in a helix-coil multiblock globule. Helical and coil parts are treated as stiff rods and self-avoiding walks of variable lengths correspondingly. The resulting field-theory takes, in addition to the conventional Zimm-Bragg parameters, also three-dimensional interaction terms into account. The appropriate differential equations which determine the self-consistent fields were solved numerically with finite element method. Three different phase states are found: open chain, amorphous globule and nematic liquid-crystalline (LC) globule. The LC-globule formation is driven by the interplay between the hydrophobic helical segments attraction and the anisotropic globule surface energy of an entropic nature. The full phase diagram of the helix-coil copolymer was calculated and thoroughly discussed. The suggested theory shows a clear interplay between secondary and tertiary structures in globular homopolypeptides.

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## I. INTRODUCTION

Significant work has been done to investigate the helix-coil transition theoretically<sup>1</sup> and computationally<sup>2,3</sup>. One of the first and well-known approaches is the Zimm-Bragg theory<sup>4</sup> which is designed for single-stranded polypeptide chains. It considers a one-dimensional Ising type model in which each segment can be in one of the two states: helical state (stiff) or coil state (flexible). The helix is stabilized by hydrogen bonds which generates an energy gain of  $-\epsilon$  for each segment in the helical state. This energy gain is partly balanced by an entropy loss  $-\Delta S$ . The free energy difference between the helical state and the coil state is therefore given by  $\Delta f = -\epsilon + T\Delta S$  for each segment.

In an  $\alpha$ -helix hydrogen bonds can be only formed between the  $i^{\text{th}}$  and the  $(i+3)^{\text{th}}$  peptide group. The formation of a hydrogen bond between the first and the third peptide group fixes the conformation of three groups. The next bond between the second and the fourth group furnishes the same energy gain but fixes only one new group and thus leads to a much smaller entropy loss. The formation of an  $\alpha$ -helix (as a simple element of the secondary structure) is therefore a cooperative process and the formation of a junction between helix and coil is energetically unfavorable. This can be modelled by an energy penalty  $\mu_J$  for each junction between two successive groups of helical and flexible segments. Similar arguments hold for all kind of helices, such that the helix formation is always a cooperative process.

It is convenient to define the following fugacities

$$s \equiv e^{-\beta\Delta f}, \quad \sigma \equiv e^{-2\beta\mu_J}, \quad (1.1)$$

where  $s$  gives the statistical weight of a helical segment compared to a coil segment. The cooperativity parameter  $\sigma$  gives the statistical weight of a junction point.  $\sigma = 1$  corresponds to  $\mu_J = 0$  and therefore to a non-cooperative system.  $\sigma \rightarrow 0$  corresponds to  $\mu_J \rightarrow \infty$  and therefore to a totally cooperative system, i.e. either the entire chain forms one big helix or no helix is formed at all. In most helix forming biopolymers  $\sigma$  is roughly  $10^{-3} - 10^{-4}$  (see e.g. ref.<sup>1</sup>).

Using a transfer matrix method<sup>1</sup> the one dimensional model can be solved exactly. The  $s$ -dependence of the fraction of stiff helical segment  $\Theta_R = N_R/N$  has a typical sigmoid-type form. With increasing cooperativity (i.e. as the parameter  $\sigma$  is reduced) the transition becomes sharper and sharper. This rather sharp crossover transition (due to the cooperativity effect) is also observed experimentally, for instance in polybenzylglutamate<sup>4</sup>.

Several extensions have been made to this one-dimensional Ising type model. It has been shown<sup>5</sup> that the transition becomes less cooperative, if the hydrogen-bonding ability of the solvent is taken into account. The helix-coil transition in grafted chains was studied<sup>6</sup> as well as the effect of an external applied force on the transition<sup>7</sup>.

Of special interest is the application of one-dimensional models to proteins, see for instance<sup>8,9</sup>. A study of the helix-coil transition including long-range electrostatic interactions<sup>10</sup> can, to some extent, explain the amount and location of helical segments in globular proteins. However, to understand how  $\alpha$ -helices (or generally secondary structure elements) are formed in the folding process of a protein and how this influences the compaction and formation of tertiary structure (and vice versa), it is necessary to combine the one-dimensional physics of the helix-coil transition with the interactions of segments which approach each other in the three-dimensional space. This enables a description

of the interplay between the *secondary structure* and the mesoscopic structure formation of the entire chain (known as *tertiary structure*).

In proteins the stiff helical parts are often hydrophobic since the hydrogen bonds stabilizing the helix composition (as opposed to coil parts) are mainly saturated (due to bond formation between the  $i^{\text{th}}$  and the  $(i + 3)^{\text{th}}$  peptide groups). This hydrophobicity causes an additional attractive interaction between stiff parts and drives the protein into a compact globular phase. Statistical analysis of the data from 41 globular proteins in native and partially folded conformational states<sup>11</sup> showed a strong correlation between the amount of secondary structure elements and compactness of the proteins. This indicates that the formation of secondary structure (for instance  $\alpha$ -helices) and the hydrophobic collapse into a compact globule occur simultaneously. This problem has been partially discussed within computer simulations of globular proteins<sup>12,13,14,15</sup>. Among other things, it has been shown<sup>13,14,15</sup> (as opposed to the earlier findings by Dill et al.<sup>12</sup>) that the compactness itself, driven by the hydrophobicity, is insufficient to generate any appreciable secondary structure. It was necessary to introduce a local conformational propensity toward  $\alpha$  - helix formation. The interplay of compaction and secondary structure leads to the formation of the specific three-dimensional tertiary structure. Computational and experimental studies of this mechanism can for instance be found in ref.<sup>16,17</sup>.

To study the interplay of helix-coil (or stiff-flexible) transition and collapse transition of the polymer into a compact globule, we have developed an approach which combines variable composition with three-dimensional excluded volume interactions using self-consistent field theory. The paper is organized as follows. In Section II we have covered the general self - consistent field theory of a helix - coil copolymeric globule. The final equations are written down in a form which is convenient for the numerical solution. Section III is devoted to the analysis of this solution. The formation of different globule structures (e.g. amorphous and liquid - crystalline (LC) globules) are studied in details. Among other things we argue that the LC - globule formation is mainly driven by the globule surface tension anisotropy. Finally, in Section IV we sketch the main results and compare them with the appropriate findings of some other authors.

## II. THEORY

In this section the derivation of the field theory is outlined. For a more detailed description see<sup>18</sup>. Regarding all three dimensional interactions and entropic contributions the helices are modelled as stiff rods. Hence for one specific microscopic composition of helical and flexible parts the system looks like a rod-coil multiblock copolymer as shown in Fig.(1). The multiblock copolymer may be composed of  $K$  rod-coil blocks. The conformation of the  $n^{\text{th}}$  rod-coil block is given by the vector-function  $\mathbf{r}_n(s)$  describing the contour of the coil, by the vector  $\mathbf{R}_n$  which gives the position of the junction point between rod and coil and the unit vector  $\mathbf{u}_n$  describes the orientation of the rod, see Fig.(1). The

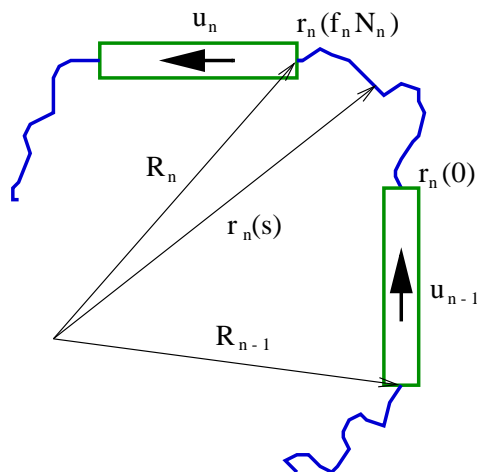


FIG. 1: Rod-coil multiblock copolymer parameterization. Two successive rod-coil blocks with ordinal numbers  $n - 1$  and  $n$  are shown. The flexible chain coordinates use the vector set  $\mathbf{r}(s)$ . The orientation of the  $n^{\text{th}}$  rod is denoted as  $\mathbf{u}_n$  and the junction point between rod and coil is given by  $\mathbf{R}_n$ .

length of the  $n^{\text{th}}$  rod-coil block in units of the segment length  $b$  is given by  $N_n$ . The fraction of the flexible segments (coil) is given by  $f_n$  and the fraction of stiff segments (rod) thus by  $1 - f_n$ . The microscopic flexible segment density

$\hat{\rho}_C(\mathbf{r})$  and stiff segment density  $\hat{\rho}_R(\mathbf{r})$  can now be defined as follows.

$$\hat{\rho}_C(\mathbf{r}) = \sum_{n=0}^K \int_0^{f_n N_n} ds \delta(\mathbf{r} - \mathbf{r}_n(s)), \quad (2.1)$$

$$\hat{\rho}_R(\mathbf{r}) = \sum_{n=0}^K \int_0^{(1-f_n)N_n} ds \delta(\mathbf{r} - \mathbf{R}_n - \mathbf{u}_n s b). \quad (2.2)$$

In addition an orientation density  $\hat{S}^{ij}(\mathbf{r})$  is introduced which is sensitive to the collective orientation of the system

$$\hat{S}^{ij}(\mathbf{r}) = \sum_{n=0}^K \int_0^{(1-f_n)N_n} ds \delta(\mathbf{r} - \mathbf{R}_n - \mathbf{u}_n s b) \left[ u^i u^j - \frac{1}{3} \delta^{ij} \right]. \quad (2.3)$$

The interaction Hamiltonian of the model can thus be written as

$$\begin{aligned} \beta H_{\text{int}}[\hat{\rho}_C, \hat{\rho}_R] &= \chi \int d^3 r \hat{\rho}_R(\mathbf{r}) \hat{\rho}_R(\mathbf{r}) + \frac{v}{2} \int d^3 r [\hat{\rho}_C(\mathbf{r}) + \hat{\rho}_R(\mathbf{r})]^2 \\ &+ \frac{w}{3!} \int d^3 r [\hat{\rho}_C(\mathbf{r}) + \hat{\rho}_R(\mathbf{r})]^3 + g \int d^3 r \text{Tr} [\hat{S}^{ij}(\mathbf{r}) \hat{S}^{ij}(\mathbf{r})], \end{aligned} \quad (2.4)$$

where  $v$  and  $w$  control the strength of the global two- and three-body interactions. The parameter  $\chi$  controls a selective two-body interaction between the stiff segments which is caused by the hydrophobic nature of the helical parts of the chain (cf. Introduction). The last term is a alignment interaction between the rods of the standard Maier-Saupe form<sup>19</sup>. The representation of this type has a wide use in the polymeric liquid-crystal context<sup>20</sup>.

The canonical partition function of the entire system can be written as the functional integral over the collective coil, rod and orientation densities,  $\rho_C(\mathbf{r})$ ,  $\rho_R(\mathbf{r})$  and  $S^{ij}(\mathbf{r})$  respectively, i.e.

$$\begin{aligned} Z(\{N_n\}, K) &= \int \mathcal{D}\rho_C(\mathbf{r}) \int \mathcal{D}\rho_R(\mathbf{r}) \int \mathcal{D}S^{ij}(\mathbf{r}) \int \prod_{n=1}^K D\mathbf{r}_n(s) d^3 R_n d^2 u_n \\ &\times \delta(\rho_C(\mathbf{r}) - \hat{\rho}_C(\mathbf{r})) \delta(\rho_R(\mathbf{r}) - \hat{\rho}_R(\mathbf{r})) \delta(S^{ij}(\mathbf{r}) - \hat{S}^{ij}(\mathbf{r})) \\ &\times \delta(|\mathbf{u}_n| - 1) \delta(\mathbf{r}_n(f_n N_n) - \mathbf{R}_n) \exp \left\{ -\frac{3}{2b^2} \int_0^{f_n N_n} ds \left( \frac{\partial \mathbf{r}_n}{\partial s} \right)^2 \right\} \\ &\times \exp \left\{ -\chi \int d^3 r \rho_R(\mathbf{r}) \rho_R(\mathbf{r}) - \frac{v}{2} \int d^3 r [\rho_C(\mathbf{r}) + \rho_R(\mathbf{r})]^2 \right. \\ &\left. - \frac{w}{3!} \int d^3 r [\rho_C(\mathbf{r}) + \rho_R(\mathbf{r})]^3 - g \int d^3 r \text{Tr} [S^{ij}(\mathbf{r}) S^{ij}(\mathbf{r})] \right\}. \end{aligned} \quad (2.5)$$

By making use of the integral representation for the  $\delta$ -function in Eq.(2.5) (which results in an appearance of external fields  $h_C(\mathbf{r})$ ,  $h_R(\mathbf{r})$  and  $h_S^{ij}(\mathbf{r})$ ) the partition function of the entire system reads

$$\begin{aligned} Z(\{N_n\}, K) &= \int \mathcal{D}\rho_C(\mathbf{r}) \int \mathcal{D}\rho_R(\mathbf{r}) \int \mathcal{D}S^{ij}(\mathbf{r}) \int \mathcal{D}h_C(\mathbf{r}) \int \mathcal{D}h_R(\mathbf{r}) \int \mathcal{D}h_S^{ij}(\mathbf{r}) \\ &\times \exp \left\{ -\chi \int d^3 r \rho_R(\mathbf{r}) \rho_R(\mathbf{r}) - \frac{v}{2} \int d^3 r [\rho_C(\mathbf{r}) + \rho_R(\mathbf{r})]^2 \right. \\ &- \frac{w}{3!} \int d^3 r [\rho_C(\mathbf{r}) + \rho_R(\mathbf{r})]^3 - g \int d^3 r \text{Tr} [S^{ij}(\mathbf{r}) S^{ij}(\mathbf{r})] \\ &+ i \int d^3 r \rho_C(\mathbf{r}) h_C(\mathbf{r}) + i \int d^3 r \rho_R(\mathbf{r}) h_R(\mathbf{r}) + i \int d^3 r S^{ij}(\mathbf{r}) h_S^{ij}(\mathbf{r}) \left. \right\} \\ &\times Z^{(0)}(\{N_n\}, K; [h_C], [h_R], [h_S^{ij}]) \quad , \end{aligned} \quad (2.6)$$

where the partition function  $Z^{(0)}$  of the non-interacting system in the external fields  $h_C$ ,  $h_R$ ,  $h_S^{ij}$  is given by

$$\begin{aligned}
Z^{(0)}(\{N_n\}, K; [h_C], [h_R], [h_S^{ij}]) &= \int \prod_{n=1}^K \mathcal{D}\mathbf{r}_n(s) d^3 R_n d^2 u_n \delta(|\mathbf{u}_n| - 1) \delta(\mathbf{r}_n(f_n N_n) - \mathbf{R}_n) \\
&\times \exp \left\{ -\frac{3}{2b^2} \int_0^{f_n N_n} ds \left( \frac{\partial \mathbf{r}_n}{\partial s} \right)^2 - i \int_0^{f_n N_n} ds h_C(\mathbf{r}_n(s)) \right. \\
&- i \int_0^{(1-f_n)N_n} ds h_R(\mathbf{R}_n + \mathbf{u}_n s) \\
&\left. - i \int_0^{(1-f_n)N_n} ds h_S^{ij}(\mathbf{R}_n + \mathbf{u}_n s) \left( u_n^i u_n^j - \frac{1}{3} \delta^{ij} \right) \right\}. \tag{2.7}
\end{aligned}$$

The composition of the system is assumed to be equilibrated with respect to the total number of stiff ( $N_R$ ) and flexible ( $N_C$ ) segments as well as to the number of junction points ( $N_J$ ) between stiff and flexible parts. Therefore the description can be reduced, i.e.  $\{N_n\}, K \rightarrow N_R, N_C, N_J$ , and it is more convenient to switch to a grand canonical partition function  $Z$  of the interacting polymer written in terms of the grand canonical partition function  $Z^{(0)}$  of the non-interacting polymer in the external fields  $h_C$ ,  $h_R$ ,  $h_S^{ij}$ , i.e.

$$\begin{aligned}
Z(\mu, \epsilon, \sigma) &= \int \mathcal{D}\rho_C(\mathbf{r}) \int \mathcal{D}\rho_R(\mathbf{r}) \int \mathcal{D}S^{ij}(\mathbf{r}) \int \mathcal{D}h_C(\mathbf{r}) \int \mathcal{D}h_R(\mathbf{r}) \int \mathcal{D}h_S^{ij}(\mathbf{r}) \\
&\times \exp \left\{ -\beta H_{\text{int}}[\rho_C, \rho_R] + i \int d^3 r \rho_C(\mathbf{r}) h_C(\mathbf{r}) + i \int d^3 r \rho_R(\mathbf{r}) h_R(\mathbf{r}) + i \int d^3 r S^{ij}(\mathbf{r}) h_S^{ij}(\mathbf{r}) \right\} \\
&\times Z^{(0)}(\mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}]). \tag{2.8}
\end{aligned}$$

In Eq.(2.8)  $\mu$  denotes the chemical potential conjugated to the whole number of segments and  $-\epsilon$  is the energy gain of a helical segments compared to coil segment. The meaning of the cooperativity parameter  $\sigma$  was discussed in the introduction.

The grand canonical partition function  $Z^{(0)}$  of the non-interacting system can be derived by using the polymeric correlation function  $\Xi^{(0)}$ , i.e.  $Z^{(0)}(\mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}]) = \int d1 d1' \Xi^{(0)}(1, 1'; \mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}])$ . The polymeric correlation function  $\Xi^{(0)}(1, 1'; \mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}])$  gives the conditional unnormalized probability of finding the first segment of the copolymer at the coordinate 1 provided that the last segment is at  $1'$ . The symbol 1 stands either for  $\mathbf{r}_1$  or for  $(\mathbf{r}_1, \mathbf{u}_1)$  depending on whether the first segment is a flexible or a stiff one. The same holds for the coordinate  $1'$  of the last segment. The polymeric correlation function is therefore the partition function of the multiblock helix-coil copolymer with two ends fixed at 1 and  $1'$ .

By using the equations of motion for the rod and coil Green functions -  $G_{\text{coil}}$  and  $G_{\text{rod}}$  - the polymeric correlation function  $\Xi^{(0)}$  can be constructed. The inverse Greens function operators are given by<sup>18</sup>

$$\hat{G}_{\text{coil}}^{-1} = \delta(\mathbf{r} - \mathbf{r}') \left( \beta\mu - \frac{b^2}{6} \nabla_r^2 + i h_C(\mathbf{r}) \right) \tag{2.9}$$

$$\hat{G}_{\text{rod}}^{-1} = \delta(\mathbf{r} - \mathbf{r}') \left( \beta(\mu - \epsilon) - \frac{b^2(\mathbf{u} \cdot \nabla_R)^2}{\beta(\mu - \epsilon)} + i h_R(\mathbf{r}) + i \overleftrightarrow{h}_S(\mathbf{r}) : \overleftrightarrow{P} \right), \tag{2.10}$$

where the tensor  $\overleftrightarrow{P}$  is given by  $P^{ij} \equiv u^i u^j - \delta^{ij}/3$ . In Eqs.(2.9) - (2.10) we have set the elementary unit lengths in coil and rod parts equal to each other (namely to  $b$ ) for simplicity. This affects some quantitative values but definitely does not alter qualitative predictions of this paper.

Knowing the inverse Green function operators the grand canonical polymeric correlation function can now be represented as the following Gaussian 2-dimensional path integral

$$\begin{aligned}
\Xi^{(0)}(1, 1'; \mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}]) &= \frac{1}{\Theta} \int \mathcal{D}\psi \mathcal{D}\varphi \psi(1) \varphi(1') \\
&\times \exp \left\{ -\frac{1}{2} \int d3 d4 \begin{pmatrix} \psi(3) \\ \varphi(3) \end{pmatrix}^T \begin{pmatrix} \hat{G}_{\text{rod}}^{-1} & -\sigma^{1/2} \\ -\sigma^{1/2} & \hat{G}_{\text{coil}}^{-1} \end{pmatrix} \begin{pmatrix} \psi(4) \\ \varphi(4) \end{pmatrix} \right\}, \tag{2.11}
\end{aligned}$$

where

$$\Theta = \int \mathcal{D}\psi \mathcal{D}\varphi \exp \left\{ -\frac{1}{2} \int d3 d4 \begin{pmatrix} \psi(3) \\ \varphi(3) \end{pmatrix}^T \begin{pmatrix} \hat{G}_{\text{rod}}^{-1} & -\sigma^{1/2} \\ -\sigma^{1/2} & \hat{G}_{\text{coil}}^{-1} \end{pmatrix} \begin{pmatrix} \psi(4) \\ \varphi(4) \end{pmatrix} \right\}. \quad (2.12)$$

The choice of  $\psi(1) \varphi(1')$  under the path integral yields one rod-coil unit as a basic building block, see Fig.(2) and Eq.(2.14). This choice assigns the coordinates (1) and (1') to  $(\mathbf{r}, \mathbf{u})$  and  $(\mathbf{r}', \mathbf{u}')$  respectively. Similarly,  $\psi(3)$  and  $\psi(4)$  are shorthand notations for  $\psi(\mathbf{r}_3, \mathbf{u}_3)$  and  $\psi(\mathbf{r}_4, \mathbf{u}_4)$ .

The inversion of the  $2 \times 2$ -matrix in Eq.(2.11) reads

$$\begin{pmatrix} \hat{G}_{\text{rod}}^{-1} & -\sigma^{1/2} \\ -\sigma^{1/2} & \hat{G}_{\text{coil}}^{-1} \end{pmatrix}^{-1} = \frac{1}{\hat{G}_{\text{rod}}^{-1} * \hat{G}_{\text{coil}}^{-1} - \sigma} \begin{pmatrix} \hat{G}_{\text{coil}}^{-1} & \sigma^{1/2} \\ \sigma^{1/2} & \hat{G}_{\text{rod}}^{-1} \end{pmatrix}. \quad (2.13)$$

The calculation of the path integral in Eq.(2.11) yields the following result

$$\begin{aligned} \Xi^{(0)}(1, 1'; \mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}]) &= \frac{\sigma^{1/2}}{\hat{G}_{\text{rod}}^{-1} * \hat{G}_{\text{coil}}^{-1} - \sigma} \\ &= \sigma^{1/2} \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}} * \left[ \hat{1} + \sigma \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}} \right. \\ &\quad \left. + \sigma^2 \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}} * \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}} + \dots \right]. \end{aligned} \quad (2.14)$$

The asterisk in Eq.(2.14) is a shorthand notation for a convolution of Green function operators. The geometric progression with a convolution as a binary relation has a clear pictorial representation, see Fig.(2). The first term of

$$\Xi_{\mu, \sigma, \epsilon}(1, 1'; [h_C], [h_R], [\vec{h}_S]) =$$

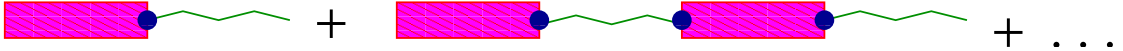


FIG. 2: Pictorial representation of the geometric progression in Eq.(2.14). One rod-coil unit constitutes the basic building block.

this series has the analytical expression  $\sigma^{1/2} \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}}$ , whereas the ratio is equal to  $\sigma \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}}$ , see also Fig.(3). The first term represents one rod-coil unit with one junction between rod and coil, hence the factor  $\sigma^{1/2}$ . If an additional building block is added, two more junctions are created, hence the factor  $\sigma$  in the ratio. This series gives a correct representation of the grand canonical polymeric correlation function.

$$\begin{array}{c} \text{Diagram: A pink bar (rod) with a blue dot at its right end, followed by a green zigzag line (coil). Below the bar, two arrows point upwards to its ends, labeled } \hat{G}_{\text{rod}} \text{ and } \hat{G}_{\text{coil}} \text{ respectively. Below these arrows is a large } \sigma \text{ symbol.} \\ \hline \text{Equation: } = \sigma \hat{G}_{\text{rod}} * \hat{G}_{\text{coil}} \end{array}$$

FIG. 3: Pictorial representation of the series ratio in Eq.(2.14): each bar (rod), zigzag line (coil) and fat dot correspond to  $\hat{G}_{\text{rod}}, \hat{G}_{\text{coil}}$ , and  $\sigma^{1/2}$  respectively.

The denominator in Eq.(2.11) can be avoided by introducing de Gennes'  $n \rightarrow 0$  trick<sup>21</sup>. Consider the two  $n$ -component vector fields  $\{\psi_\alpha, \varphi_\alpha\}$ , where  $\alpha = 1, 2, \dots, n$ . Then Eq.(2.11) can be formally rewritten as

$$\begin{aligned} \Xi^{(0)}(1, 1'; \mu, \epsilon, \sigma; [h_C], [h_R], [h_S^{ij}]) &= \lim_{n \rightarrow 0} \prod_{\alpha=1}^n \int \mathcal{D}\psi_\alpha \mathcal{D}\varphi_\alpha \psi_1(1) \varphi_1(1') \\ &\times \exp \left\{ -\frac{1}{2} \int d^3d^4 \sum_{\alpha=1}^n \begin{pmatrix} \psi_\alpha(3) \\ \varphi_\alpha(3) \end{pmatrix}^\top \begin{pmatrix} \hat{G}_{\text{rod}}^{-1} & -\sigma^{1/2} \\ -\sigma^{1/2} & \hat{G}_{\text{coil}}^{-1} \end{pmatrix} \begin{pmatrix} \psi_\alpha(4) \\ \varphi_\alpha(4) \end{pmatrix} \right\}. \end{aligned} \quad (2.15)$$

Integrations over the external fields  $h_C$ ,  $h_R$ ,  $h_S^{ij}$ , over the densities  $\rho_C(\mathbf{r})$ ,  $\rho_R(\mathbf{r})$ ,  $S^{ij}(\mathbf{r})$  and over all endpoints  $\{1, 1'\}$  yield the final field theoretic representation of the grand canonical partition function

$$\begin{aligned} Z(\mu, \epsilon, \sigma) &= \lim_{n \rightarrow 0} \prod_{\alpha=1}^n \int \mathcal{D}\psi_\alpha \mathcal{D}\varphi_\alpha \left[ \int d^3r d^2u \psi_1(\mathbf{r}, \mathbf{u}) \right] \left[ \int d^3r' \varphi_1(\mathbf{r}') \right] \\ &\times \exp \left\{ -\frac{1}{2} \sum_{\alpha=1}^n \int d^3r d^2u \psi_\alpha(\mathbf{r}, \mathbf{u}) \left[ \beta(\mu - \epsilon) - \frac{b^2 (\mathbf{u} \cdot \nabla_r)^2}{\beta(\mu - \epsilon)} \right] \psi_\alpha(\mathbf{r}, \mathbf{u}) \right. \\ &- \frac{1}{2} \sum_{\alpha=1}^n \int d^3r \varphi_\alpha(\mathbf{r}) \left[ \beta\mu - \frac{b^2}{6} \nabla_r^2 \right] \varphi_\alpha(\mathbf{r}) \\ &- \frac{\chi}{4} \int d^3r \left[ \sum_{\alpha=1}^n \int d^2u \psi_\alpha^2(\mathbf{r}, \mathbf{u}) \right]^2 \\ &- \frac{v}{8} \int d^3r \left[ \sum_{\alpha=1}^n \int d^2u \psi_\alpha^2(\mathbf{r}, \mathbf{u}) + \sum_{\alpha'=1}^n \varphi_{\alpha'}^2(\mathbf{r}) \right]^2 \\ &- \frac{w}{48} \int d^3r \left[ \sum_{\alpha=1}^n \int d^2u \psi_\alpha^2(\mathbf{r}, \mathbf{u}) + \sum_{\alpha'=1}^n \varphi_{\alpha'}^2(\mathbf{r}) \right]^3 \\ &+ \sigma^{1/2} \sum_{\alpha=1}^n \int d^3r d^2u \psi_\alpha(\mathbf{r}, \mathbf{u}) \varphi_\alpha(\mathbf{r}) \\ &\left. - \frac{g}{4} \sum_{\alpha=1}^n \sum_{\alpha'=1}^n \int d^3r d^2u d^2u' P_2(\mathbf{u} \cdot \mathbf{u}') \psi_\alpha^2(\mathbf{r}, \mathbf{u}) \psi_{\alpha'}^2(\mathbf{r}, \mathbf{u}') \right\}, \end{aligned} \quad (2.16)$$

where the second Legendre polynomial is given by

$$P_2(\theta) = \frac{1}{2} (3 \cos^2 \theta - 1). \quad (2.17)$$

To evaluate the partition function  $Z(\mu, \epsilon, \sigma)$  the self-consistent field approximation is used<sup>22</sup>. In the self-consistent field approximation fluctuations are neglected and the functional integral over the fields in Eq.(2.16) is integrated by steepest descent. The saddle point solutions for  $\varphi_\alpha(\mathbf{r})$  and  $\psi_\alpha(\mathbf{r}, \mathbf{u})$  are chosen such that the effective grand potential keeps the full symmetry of the Hamiltonian in replica space, i.e. it is invariant under rotations in replica space. This is the case for (see ref.<sup>21</sup>)

$$\begin{aligned} \psi_\alpha(\mathbf{r}, \mathbf{u}) &= n_\alpha \psi(\mathbf{r}, \mathbf{u}) \\ \varphi_\alpha(\mathbf{r}) &= n_\alpha \varphi(\mathbf{r}), \end{aligned} \quad (2.18)$$

where  $\mathbf{n}$  is a unit vector such that  $\sum_{\alpha=1}^n n_\alpha^2 = 1$ .

In order to make the problem more tractable we expand  $\psi(\mathbf{r}, \mathbf{u})$  in spherical harmonics,  $\psi(\mathbf{r}, \mathbf{u}) = \sum_{l,m} \psi_{lm}(\mathbf{r}) Y_{lm}(\mathbf{u})$ , (see e.g. ref.<sup>23</sup>). Since the solution for  $\psi(\mathbf{r}, \mathbf{u})$  must respect uniaxial and cylindrical symmetry, the expansion reduces to Legendre polynomials, i.e.  $m \equiv 0$ . This expansion is truncated to the lowest nontrivial order<sup>24</sup>

$$\psi(\mathbf{r}, \mathbf{u}) \approx \left( \frac{1}{4\pi} \right)^{1/2} \psi_0(\mathbf{r}) + \left( \frac{5}{4\pi} \right)^{1/2} \psi_2(\mathbf{r}) P_2(\mathbf{u} \cdot \mathbf{n}_z), \quad (2.19)$$

where  $\mathbf{n}$  is the main direction along which the rods in the core of the globule are aligned, if the system forms an anisotropic globule with aligned rods. If they are not aligned and the system forms an amorphous globule, only the first term in the expansion in Eq.(2.19) differs from zero. On the other hand, the second term in Eq.(2.19) is responsible for the nematic LC-order. The main direction of alignment  $\mathbf{n}$  can be chosen arbitrarily without loss of generality, since a change in alignment direction only corresponds to a rotation of the complete globule in the laboratory coordinate frame. Thus we choose  $\mathbf{n}$  directed along the  $z$ -axis of the  $(x, y, z)$  laboratory frame, i.e.  $\mathbf{n} = \mathbf{n}_z$ . This expansion allows us to perform the  $\mathbf{u}$ -integrations.

The resulting effective saddle point grand potential  $\Omega(\mu, \epsilon, \sigma)$  can now be calculated. It is given in terms of the saddle point fields  $\psi_0(\mathbf{r})$ ,  $\psi_2(\mathbf{r})$  and  $\varphi(\mathbf{r})$  by

$$\begin{aligned}
\beta\Omega(\mu, \epsilon, \sigma) = & \frac{\beta(\mu - \epsilon)}{2} \int d^3r [\psi_0^2(\mathbf{r}) + \psi_2^2(\mathbf{r})] \\
& - \frac{b^2}{210\beta(\mu - \epsilon)} \int d^3r \left\{ 35\psi_0(\mathbf{r})\nabla_r^2\psi_0(\mathbf{r}) \right. \\
& + 14\sqrt{5}\psi_0(\mathbf{r})[2\partial_z^2 - \partial_x^2 - \partial_y^2]\psi_2(\mathbf{r}) \\
& + \psi_2(\mathbf{r})[25\partial_x^2 + 25\partial_y^2 + 55\partial_z^2]\psi_2(\mathbf{r}) \left. \right\} \\
& + \frac{1}{2} \int d^3r \varphi(\mathbf{r}) \left[ \beta\mu - \frac{b^2}{6}\nabla_r^2 \right] \varphi(\mathbf{r}) \\
& + \frac{\chi}{4} \int d^3r [\psi_0^2(\mathbf{r}) + \psi_2^2(\mathbf{r})]^2 \\
& + \frac{v}{8} \int d^3r [\varphi^2(\mathbf{r}) + \psi_0^2(\mathbf{r}) + \psi_2^2(\mathbf{r})]^2 \\
& + \frac{w}{48} \int d^3r [\varphi^2(\mathbf{r}) + \psi_0^2(\mathbf{r}) + \psi_2^2(\mathbf{r})]^3 \\
& - 2\sqrt{\pi\sigma} \int d^3r \varphi(\mathbf{r})\psi_0(\mathbf{r}) \\
& + \frac{g}{245} \int d^3r \left\{ \psi_2(\mathbf{r}) [7\psi_0(\mathbf{r}) + \sqrt{5}\psi_2(\mathbf{r})] \right\}^2.
\end{aligned} \tag{2.20}$$

The coil and rod densities as well as the orientation density are given by the following relations

$$\begin{aligned}
\rho_C(\mathbf{r}) &= \frac{1}{2}\varphi^2(\mathbf{r}) \\
\rho_R(\mathbf{r}) &= \frac{1}{2} \int d^2u \psi^2(\mathbf{r}, \mathbf{u}) \simeq \frac{1}{2} [\psi_0^2(\mathbf{r}) + \psi_2^2(\mathbf{r})] \\
S(\mathbf{r}) \equiv S^{zz}(\mathbf{r}) &= \frac{1}{3} \int d^2u P_2(\cos\theta) \psi^2(\mathbf{r}, \mathbf{u}) \\
&\simeq \frac{2}{\sqrt{5}} \psi_2(\mathbf{r}) [\psi_0(\mathbf{r}) + \sqrt{5}\psi_2(\mathbf{r})].
\end{aligned} \tag{2.21}$$

Functional minimization of Eq.(2.20) with respect to  $\psi_0(\mathbf{r})$ ,  $\psi_2(\mathbf{r})$  and  $\varphi(\mathbf{r})$  yields a set of three coupled partial differential equations, which are solved numerically with the finite element tool kit Gascoigne<sup>25</sup>. The results are extensively discussed in the next section.

### III. RESULTS

In this section the numerical results for the full set of equations describing a rod-coil multiblock copolymer with a variable composition of stiff and flexible segments are presented. The segment length is set to  $b = 1$ . In addition, all energies such as  $\epsilon$ ,  $\mu$  and also the saddle point free energy  $F$  are given in units of  $k_B T$ . In this section this will not be indicated in order to avoid complicated notation. Eq.(2.20) describes the copolymer in a grand-canonical representation. In the grand-canonical ensemble the total number of segments of the polymer  $N$  is not fixed but its mean value is determined by equilibrium conditions.

A real polymer has a fixed length. In order to ensure this fixed length  $N$ , the chemical potential  $\mu$  is - for each set of physical parameters  $(v, w, \chi, g, \epsilon, \sigma)$  - tuned such that the equilibrium value of  $N$  is equal to the desired one. The

total number of segments  $N = N_{\text{coil}} + N_{\text{rod}}$  is calculated by numerical integration over the rod and coil densities given by Eq.(2.21). For a given set of parameters,  $N(\mu)$  can be computed<sup>24</sup> and a typical example of this curve is shown in Fig.(4). For  $\mu \rightarrow 0$  the total number of segments  $N$  diverges. This corresponds to the  $N \sim \mu^{-1}$  behavior which is

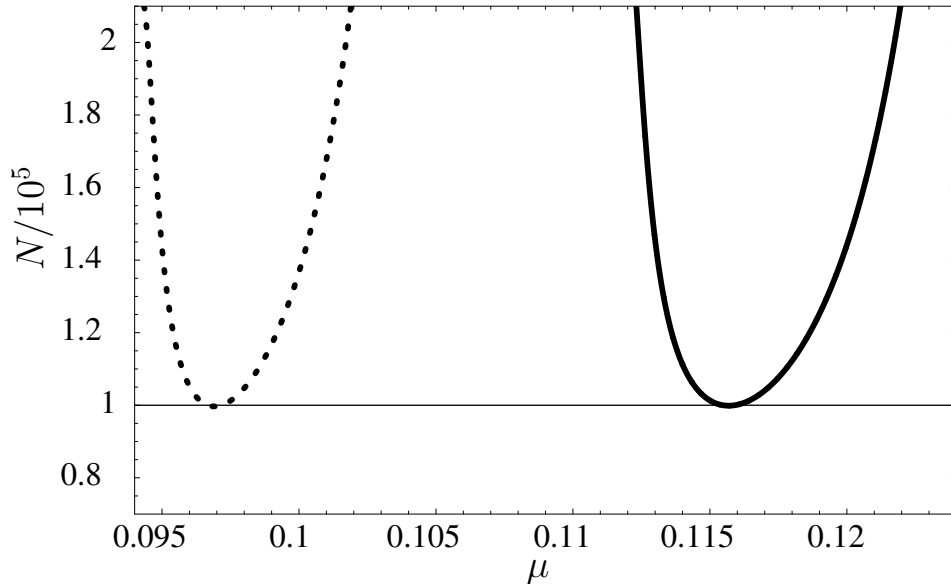


FIG. 4:  $N$  as a function of  $\mu$  for  $w = 1$ ,  $v = -0.2$  and  $\sigma = 10^{-4}$ . The dotted curve corresponds to  $\epsilon = 0.08$  and  $\chi = 0$ . The continuous curve corresponds to  $\epsilon = 0.1$  and  $\chi = 0.0138$ .

well-known for a  $\Theta$ -solvent chain<sup>26</sup>. The divergence of  $N$  at a specific value  $\mu$  on the right hand side of the minimum corresponds to a fully collapsed infinite globule and has been discussed first by Kholodenko and Freed<sup>21</sup>. These two branches of  $N(\mu)$  meet each other in the minimum of  $N(\mu)$  which can be associated with the coil-globule transition point, as will be shown in the next section. Since  $N$  is always fixed by tuning  $\mu$ , it is possible to distinguish from a plot like the one shown in Fig.(4) whether the system is left of the coil-globule transition point (i.e. in the open chain regime) or right of the transition point (i.e. in the globular regime). However, for fixed  $N$ , it is necessary to choose one of the two branches. Since this work focuses on the study of globular structures, the numerical calculations are always restricted to the right branch including the minimum. The self-consistent field theory is only expected to give good results for this branch since fluctuations are neglected.

The three-body interaction parameter  $w$  is chosen to be  $w = 1$  throughout the entire paper and the two-body interaction constant  $v$  is always negative to ensure that the system stays in the globular regime (up to the transition point).

As a first step the pure homopolymer globule case<sup>21</sup> has been studied in order to test the numerical routines. For this end one should simply set  $\psi_0 = \psi_2 = 0$  in Eq.(2.20). Here we are not going to discuss these results in detail. It is pertinent only to note that the resulting numerical solution fully supports the following well known theoretical results. The critical value of the two-body interaction constant,  $v$ , scales as  $|v_c| \sim N^{-1/2}$ , whereas the maximal globule density in the critical point behaves as  $\rho_{\text{crit}} \sim N^{-1/2}$ .

A short remark on the terminology that will be used below is necessary at this point. The terms phase and transition will be used frequently although the system is a polymer of finite length. All transitions are therefore crossovers of finite width with continuous order parameters. It is nevertheless common now as applied to "soft matter" to use the term "phase" to distinguish the different structural states of a polymer and to refer to the crossover between these states as a "transition".

### A. Coil-globule transition

The rod-coil multiblock copolymer shows a coil-globule transition similar to the one of a homopolymer. To demonstrate this, the interactions which are specific for the stiff segments are set to zero, that is  $\chi = g = 0$ . In addition, the energy gain per stiff segment is set to zero ( $\epsilon = 0$ ) and it is assumed that there is no cooperativity in the formation of stiff segments ( $\sigma = 1$ ). The two-body interaction constant  $v$  is varied. The transition point between coil and globule



is defined to be the minimum of the  $N(\mu)$ -curve as it was explained above. The length of the polymer is fixed at  $N = 550$ . Fig.(5) shows the profile of the total density  $\rho(\mathbf{r})$  of the copolymer as a function of radial distance from the center. The total density  $\rho(\mathbf{r})$  at each point is given by

$$\rho(\mathbf{r}) = \rho_C(\mathbf{r}) + \rho_R(\mathbf{r}) = \frac{1}{2}\varphi^2(\mathbf{r}) + \frac{1}{2}\psi_0^2(\mathbf{r}) + \frac{1}{2}\psi_2^2(\mathbf{r}). \quad (3.1)$$

As can be seen from Fig.(5), the density profile becomes broader with decreasing  $|v|$ . At  $v = -0.5$  the copolymer is

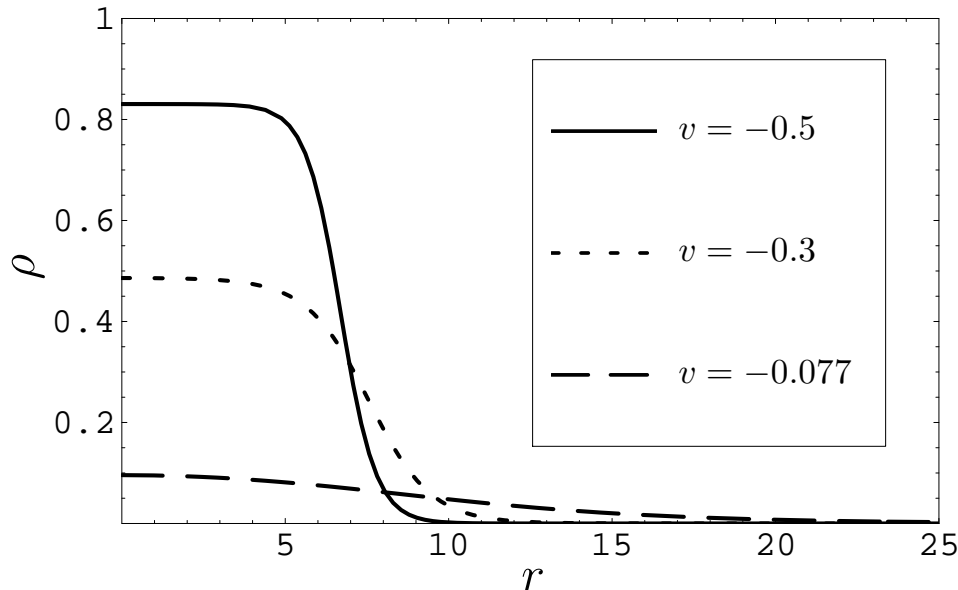


FIG. 5: This plot shows the radial density profile of the entire copolymer in radial direction for different values of  $v$ . The dashed curve for  $v = -0.077$  corresponds to the coil-globule transition point.

deep in the globular state with a big plateau of almost constant density and a rather small surface layer of decreasing density. At the transition point  $v = -0.077$  the plateau basically vanished and the surface layer becomes very broad. To further illustrate the structural change, Fig.(6) shows a colour-coded plot of the local density in  $\varrho$ - $z$  space, where  $\varrho$  denotes the radial direction and  $z$  the axial direction in cylindrical coordinates. The center of the globule is located at the bottom left corner of each picture. The pictures on the left show the local density of flexible segments and the pictures on the right correspond to the local density of stiff segments. Red indicates high density and dark blue zero density. In the upper two plots the copolymer is at the transition point ( $v = -0.077$ ). In the lower two plots it is deep in the globular state ( $v = -0.5$ ).

A much clearer indication that  $v = -0.077$  corresponds indeed to a transition point can be seen from Fig.(7), where the globule radius is plotted versus  $v$ . The globule radius is defined as the point  $R$  in radial direction at which the density  $\rho(R)$  has decreased to  $\rho(R) = 10^{-3}\rho_0$ , where  $\rho_0$  is the maximum density at the center of the globule. The radius  $R$  shows a rapid increase when  $v = -0.077$  is approached. Note, that the copolymer is finite (here:  $N=550$ ) and therefore all transitions are crossovers as discussed above.

## B. Helix-coil transition

In this section the fraction of stiff segments is investigated as a function of the energy gain per stiff segment  $\epsilon$ . This is similar to the helix-coil transition described by the Zimm-Bragg model<sup>4</sup>. A major difference is that the model used here is a three-dimensional model of the polymer including interactions, whereas the Zimm-Bragg model and its extensions are one-dimensional models with no three-dimensional interactions and no explicit entropy term. On the other hand, the Zimm-Bragg model can be solved exactly, whilst the self-consistent field treatment of the three-dimensional model is a mean-field approach which neglects fluctuations.

Two different regimes will be discussed in the following: a low cooperativity regime with  $\sigma$  in the range  $0.05 - 1$  and a high cooperativity regime with  $\sigma$  in the range  $7 \cdot 10^{-3} - 10^{-4}$ . Remember, that  $\sigma = 1$  means no cooperativity and  $\sigma = 0$  means total cooperativity. Throughout this section  $\chi$  and  $g$  are set to zero. There are therefore no specific

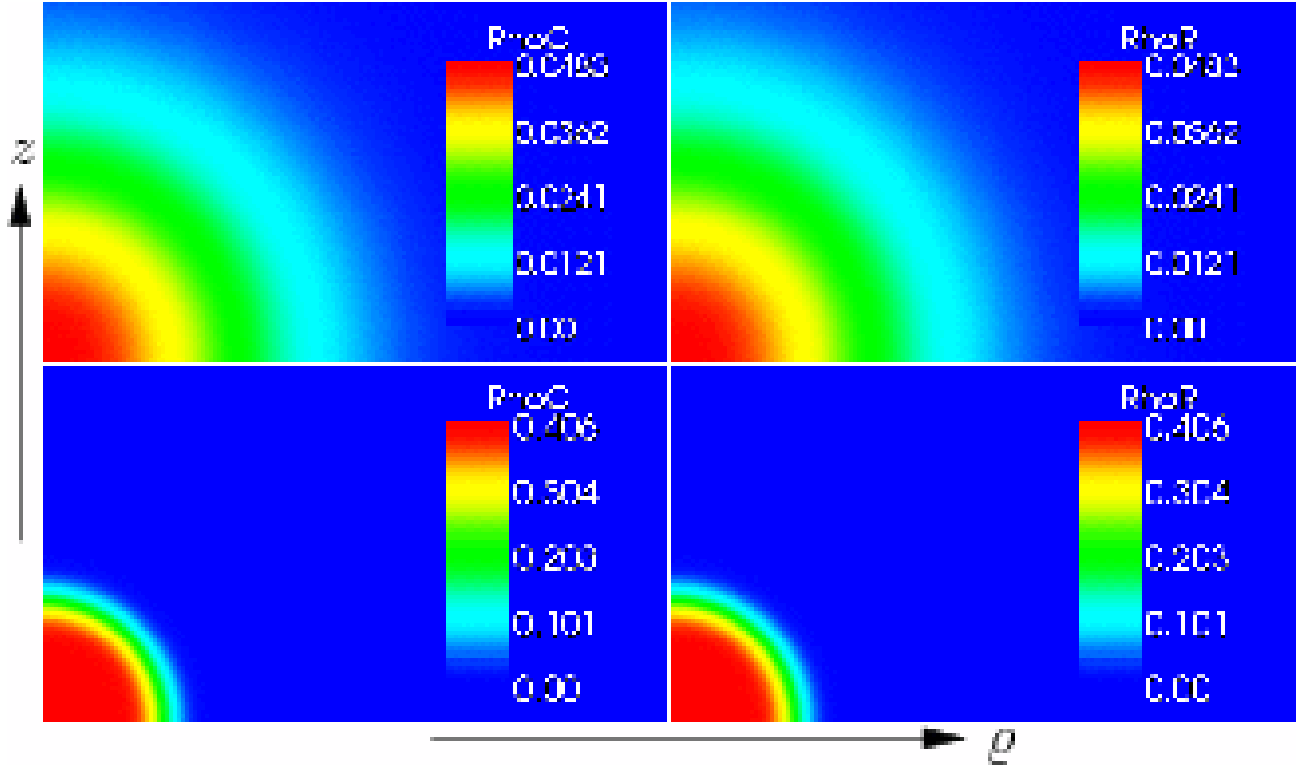


FIG. 6: The density of flexible and stiff (helical) segments are shown on the left and on the right panels respectively.  $v = -0.077$  corresponds to the upper plots and  $v = -0.5$  to the lower plots.

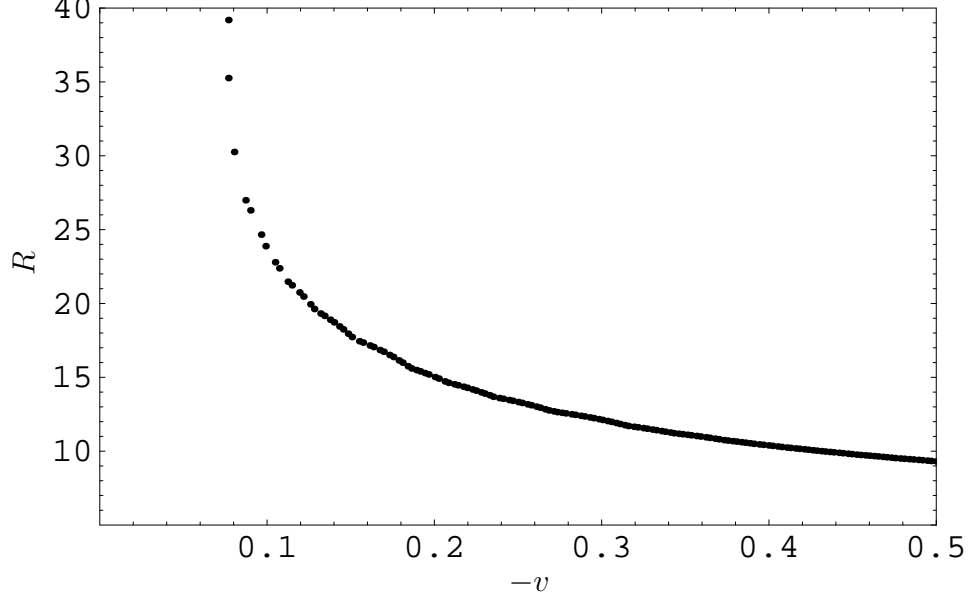


FIG. 7: The globule radius  $R$  is plotted as a function of  $v$ .

interactions between the stiff segments. The only interactions are attractive two-body interactions and repulsive three-body interactions between all segments. Fig.(8) shows how the fraction of stiff segments  $\Theta_R$  depends on  $\epsilon$  for different values of  $\sigma$  in the range  $0.05 - 1$ . Even for small cooperativity, the slope clearly depends on  $\sigma$  and gets larger with increasing cooperativity (decreasing  $\sigma$ ).

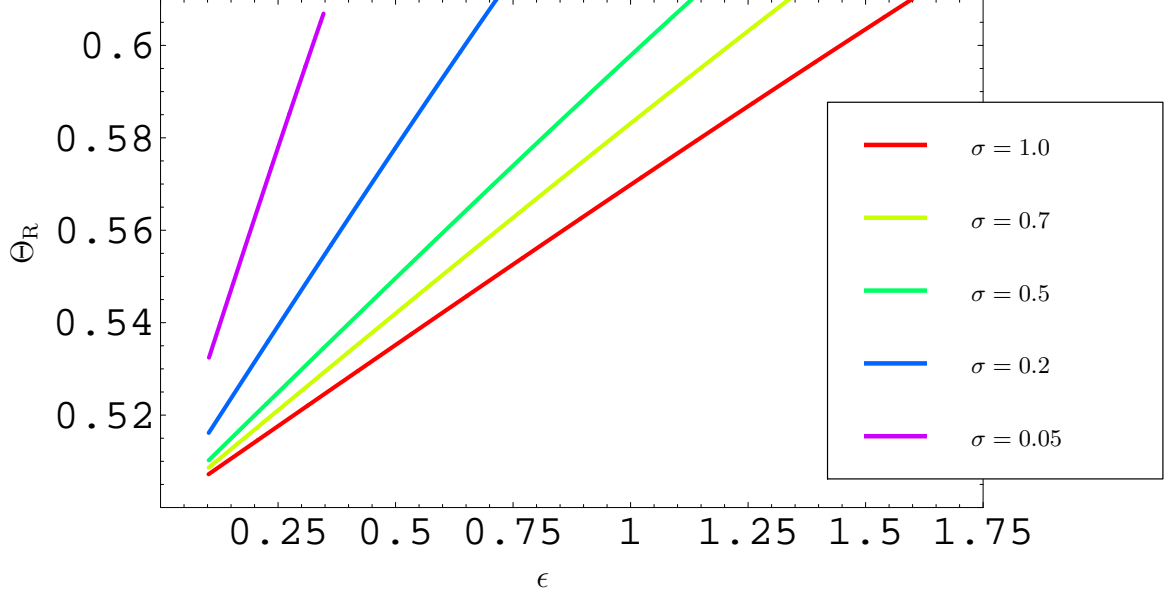


FIG. 8: The fraction of stiff segments  $\Theta_R$  is plotted as a function of energy gain  $\epsilon$  per stiff segments for small (and zero) cooperativity.  $v = -0.025$  and  $N = 2.5 \cdot 10^4$ .

The high cooperativity regime is shown in Fig.(9). The slope of the  $\Theta_R(\epsilon)$ -curves increases with decreasing  $\sigma$  as

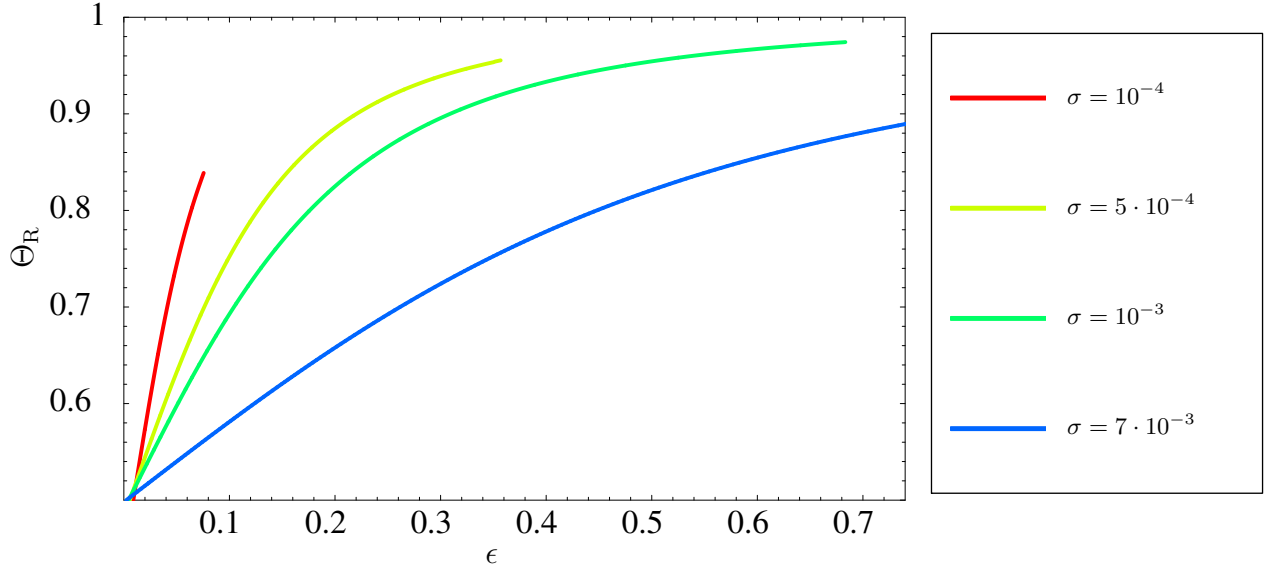


FIG. 9: The fraction of stiff segments  $\Theta_R$  is plotted as a function of  $\epsilon$  for high cooperativity.  $v = -0.2$  and  $N = 10^5$ .

expected. Especially for  $\sigma = 10^{-3}$  (green curve) it can be seen that the curve is asymptotically approaching  $\Theta_R = 1$ . The curves for  $\sigma = 10^{-4}$ ,  $5 \cdot 10^{-4}$  and  $10^{-3}$  end at a certain value of  $\epsilon$ . These values correspond to the coil-globule transition point. This can be explained as follows. If there is no additional selective interaction energy which favors a compactification of the stiff segments (i.e.  $\chi = g = 0$ ), the stiffening of parts of the chain due to an increase of  $\Theta_R$  with increasing  $\epsilon$  pushes the chain segments further apart from each other and therefore leads to a more open

structure. From a certain value of  $\epsilon$  on, the system is thus pushed into the open chain regime. For higher cooperativity this effect is stronger, since the system forms less junction points and hence on average longer rods. For smaller  $\sigma$  the coil-globule transition point is therefore reached at smaller values of  $\Theta_R$  and  $\epsilon$ .

To illustrate this stiffening, in Fig.(10) the average rod length  $L_R$  is plotted as a function of  $\epsilon$  for  $\sigma = 10^{-4}$ . In

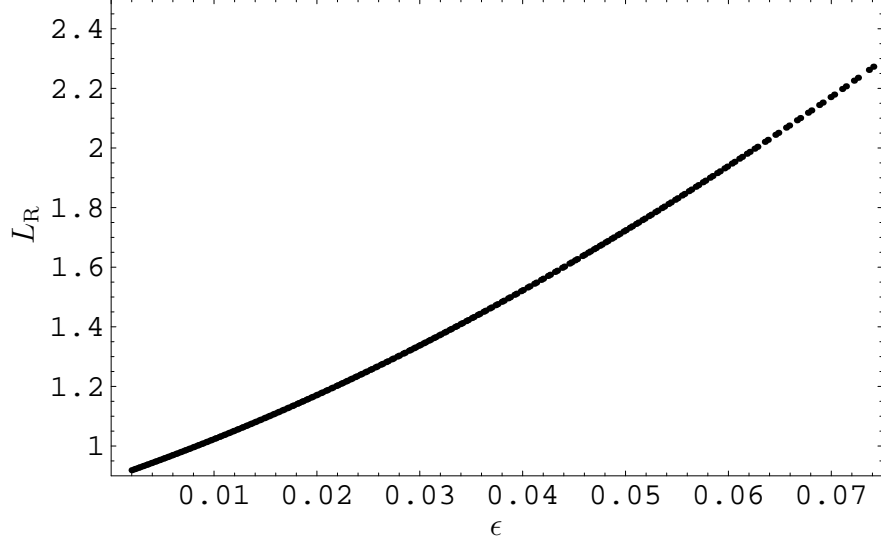


FIG. 10: The average rod length  $L_R$  is plotted as a function of  $\epsilon$  for  $\sigma = 10^{-4}$ ,  $v = -0.2$  and  $N = 10^5$ .

units of  $b$  the average rod length  $L_R$  is given by the total number of stiff segments divided by half the total number of junction points between stiff rod and flexible chain. In the self-consistent field theory approach  $L_R$  is given by

$$\frac{L_R}{b} = \frac{\int_0^\infty d\varrho \varrho \int_{-\infty}^\infty dz [\psi_0^2(\varrho, z) + \psi_2^2(\varrho, z)]}{\int_0^\infty d\varrho \varrho \int_{-\infty}^\infty dz \varphi(\varrho, z) \psi_0(\varrho, z)}. \quad (3.2)$$

Fig.(10) shows that for  $\epsilon = 0$  the average rod length is roughly equal to 1. For  $\epsilon > 0$  the cooperativity effect sets in and the average rod length increases up to  $L_R \approx 2.3$ . At this value the stiffening of parts of the chain is strong enough to drive the polymer in the open chain regime.

It is of interest to compare the results of this three-dimensional model with the exact one-dimensional Zimm-Bragg model discussed in Introduction. This is done in Fig.(11) for  $\sigma = 10^{-3}$ . Note, that in the Zimm-Bragg language the  $\epsilon$  used here corresponds to  $-\Delta f = \ln s$ . In the Zimm-Bragg model the increase of  $\Theta_R$  is steeper. This can be explained by the fact that in the three-dimensional model the entropy of the flexible and the stiff segments is explicitly taken into account, which hinders the generation of stiff segments. On the other hand, the mean-field character of the three-dimensional model might also weaken the cooperativity effect.

### C. Transition from amorphous to liquid-crystalline globule

The main focus of this work lies on the crossover from a disordered amorphous globule with a low or moderate fraction of stiff segments to an ordered liquid-crystalline globule with a very high fraction of stiff segments. In Fig.(12), on the left, the fraction of stiff segments  $\Theta_R$  is plotted as a function of the selective two-body interaction parameter  $\chi$ , which controls the strength of the additional interaction between stiff segments and therefore models selective solvent conditions (hydrophobicity). On the right the nematic order parameter  $S$  is plotted as a function of  $\chi$ . The nematic order parameter is given by

$$\begin{aligned} S &= \frac{1}{3N} \int d^3r \int d^2u P_2(\cos \theta) \psi^2(\mathbf{r}, \mathbf{u}) \\ &= \frac{2}{\sqrt{5}N} \int d^3r \psi_2(\mathbf{r}) [\psi_0(\mathbf{r}) + \sqrt{5}\psi_2(\mathbf{r})]. \end{aligned} \quad (3.3)$$

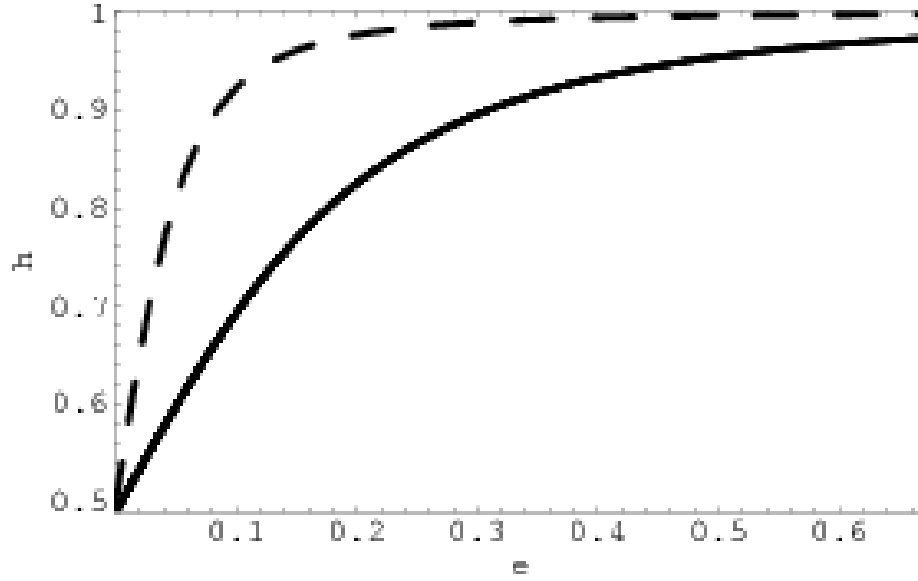


FIG. 11:  $\Theta_R$  is plotted as a function of  $\epsilon$  for  $\sigma = 10^{-3}$ . The continuous curve shows the numerical result for  $v = -0.2$  and  $N = 10^5$ . The dashed curve shows the result of the one-dimensional Zimm-Bragg theory.

Throughout the entire section, the non-selective two-body interaction parameter is set to  $v = -0.2$ . The two plots in Fig.(12) demonstrate that the onset of nematic order and the increase in the fraction of stiff segments occur simultaneously.

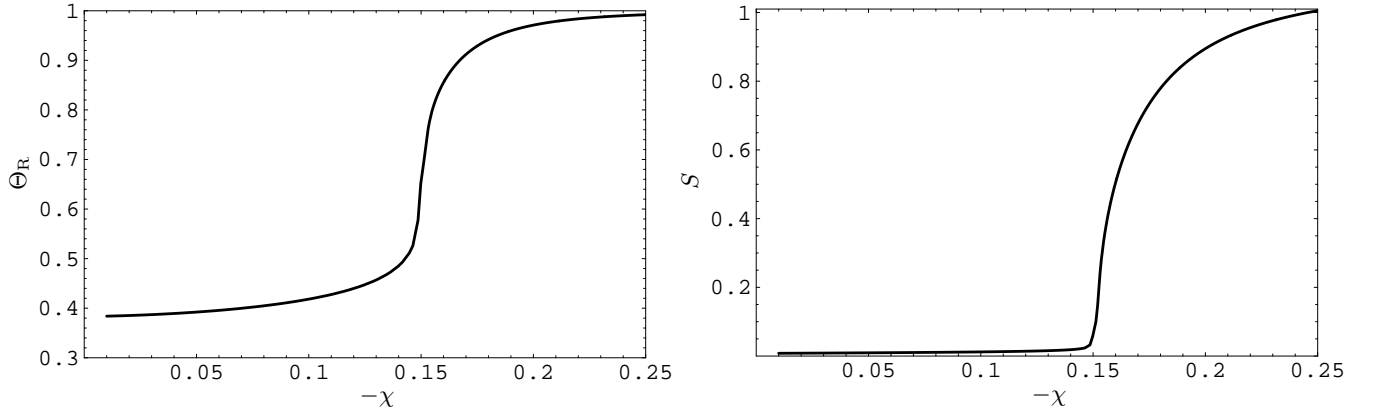


FIG. 12: The fraction of stiff segments  $\Theta_R$  (left) and the nematic order parameter  $S$  (right) are plotted as functions of  $\chi$  for  $\sigma = 10^{-4}$ ,  $N = 9.5 \cdot 10^3$  and  $\epsilon = g = 0$ .

This transition occurs without an explicit angle-dependent alignment interaction, that is  $g = 0$ . The transition is triggered by a subtle interplay of the entropy contribution (surface energy), represented by the derivative terms in Eq.(2.20), and bulk interaction energy, represented by the  $\chi$ -term. This surface energy has an entropic nature since the conformational set of surface segments is constrained. In a simple homopolymer globule it is isotropic<sup>22</sup>. For the rod-coil copolymer the surface energy is anisotropic and the surface tension in  $\varrho$ -direction is smaller than the one in  $z$ -direction. That is why the system tries to maximise its lateral surface in  $\varrho$ -direction and minimize it in  $z$ -direction, i.e. a nematic, cigar shaped, liquid-crystalline globule is formed.

To demonstrate how the shape of the globule changes during the transition, Fig.(13) shows a colour-coded plot of the local density in  $\varrho$ - $z$  space. The center of the globule is in the bottom left corner of each picture.  $\varrho$  is increasing from left to right and  $z$  is increasing from bottom to top. Red indicates high density and dark blue zero density. In Fig.(13) a different set of parameters is chosen:  $\sigma = 10^{-4}$ ,  $N = 10^5$  and  $\epsilon = 0.1$ . Below, it will be discussed in detail

how the nature of the crossover changes with  $\sigma$ ,  $\epsilon$  and  $N$ . The values of  $\chi$  in Fig.(13) are chosen such that the top

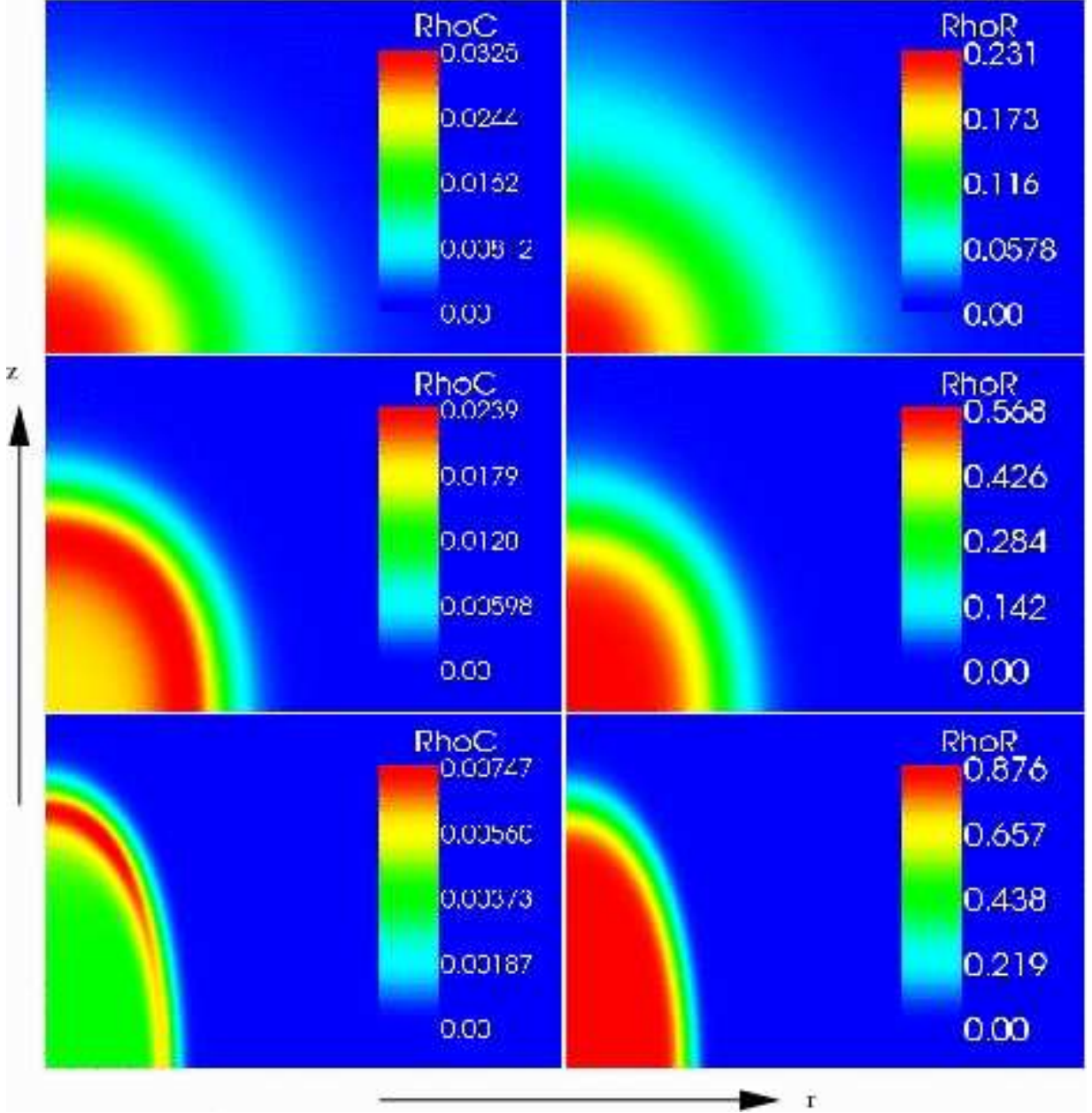


FIG. 13: The density of the flexible segments is shown on the left and the density of the stiff segments on the right.  $\sigma = 10^{-4}$ ,  $\epsilon = 0.1$  and  $N = 10^5$  for all plots.  $\chi = -0.0138$  in the top line,  $\chi = -0.0812$  in the middle line and  $\chi = -0.18$  in the bottom line.

two pictures ( $\chi = -0.0138$ ) show the system at the transition point between coil and globule, the middle two pictures ( $\chi = -0.0812$ ) show the system at the transition point between amorphous and liquid-crystalline globule (as defined below) and the bottom two pictures ( $\chi = -0.18$ ) show the system deep in the liquid-crystalline globule phase. The transition from amorphous to nematic liquid-crystalline globule is a crossover of finite width and it is a rather obvious choice, to define the transition point as the inflection point of the  $S(\chi)$ -curve in Fig.(12). At the transition point between coil and globule the system is spherical and has a very broad surface layer of decaying density. Although the density of the helical segments shown on the right is higher than the density of the flexible segments shown on the left, their distribution and the shape of the profile is very similar.

At the transition point between amorphous and liquid-crystalline globule the system adopts a slightly cylindrical shape indicating the onset of nematic order. It can also be seen that the density maximum of the flexible segments

is not in the center of the globule denoting a repulsion of flexible segments from the center to the surface layer. The surface layer is now much narrower. Deep in the liquid-crystalline phase the globule has developed a strongly asymmetric cylindrical shape indicating strong nematic order. The repulsion of flexible segments from the center towards the surface layer can be seen clearly and the surface layer is now very narrow.

### 1. $N$ -dependence

In this subsection we study how the total chain length  $N$  influences the transition from amorphous to liquid-crystalline globule. Fig.(14) shows the fraction of stiff segments as a function of  $\chi$  for four different chain lengths. The crossover from an amorphous globule with moderate number of stiff segments to a liquid-crystalline globule with very high number of a stiff segments becomes sharper with decreasing chain length, which, at first sight, is a rather unusual and surprising behavior.

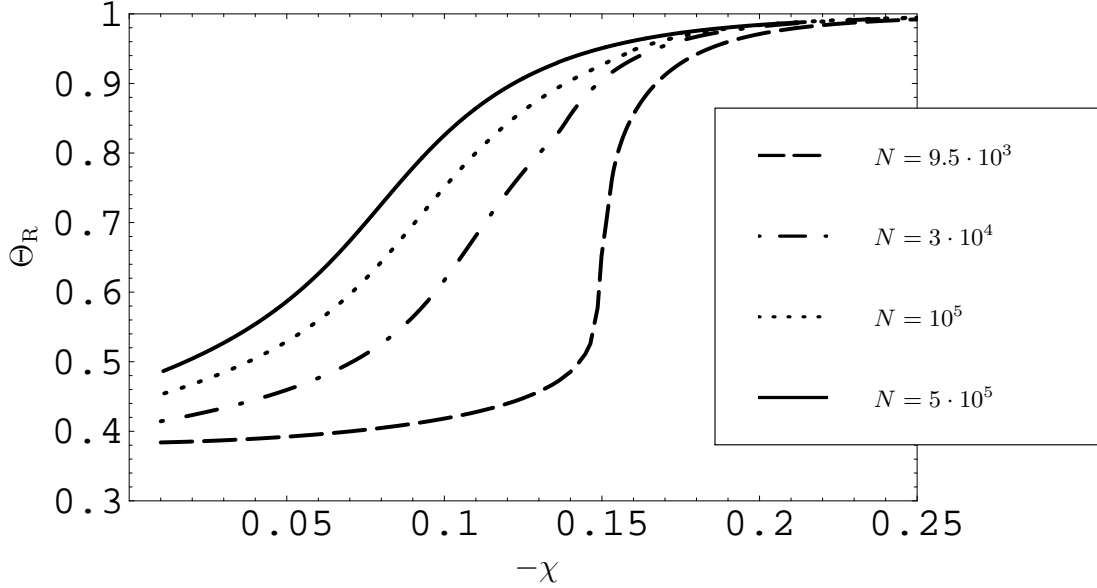


FIG. 14: The fraction of stiff segments  $\Theta_R$  is plotted as a function of  $\chi$  for different chain lengths. The crossover becomes sharper with decreasing chain length.

Fig.(15) shows the nematic order parameter  $S$  as a function of  $\chi$  for the four chain lengths. It can be seen that the increase in the order parameter is stronger for shorter chains. For  $N = 5 \cdot 10^5$  and  $\chi = -0.214$  the system is already so deep in the globular phase that the corresponding value of  $\mu$ , which keeps the chain length fixed at  $N = 5 \cdot 10^5$ , is very close to the value at which  $N(\mu)$  diverges (see Fig.(4)). The tuning of the chemical potential  $\mu$  to ensure fixed chain length  $N$  becomes therefore numerically impossible for higher values of  $|\chi|$ . Although it might be difficult to see, the corresponding  $\Theta_R(\chi)$ -curve in Fig.(14) also ends at  $\chi = -0.214$ .

To demonstrate how the shape of the liquid-crystalline globule changes with chain length  $N$ , Fig.(16) shows colour-coded density plots of  $\rho_C$  and  $\rho_R$  for the four different values of the chain length at  $\chi = -0.18$ . The plots illustrate that the system changes from a cigar-like shape for  $N = 10^4$  towards an almost cylindrical shape for  $N = 5 \cdot 10^5$ . Fig.(16) also demonstrates that the surface layer becomes smaller for larger systems, which indicates that a larger system is deeper in the globular state at the same value of  $\chi$  and  $v$  but at the same time showing less nematic order.

With increasing system size  $N$  the liquid-crystalline globule phase eventually dies out (for  $g = 0$ ) because in the limit  $N \rightarrow \infty$  the contribution of the surface terms in Eq.(2.20) vanishes. Since for  $g = 0$  these terms are the only non-spherical symmetric terms, the system cannot adopt a liquid-crystalline globular state any more. Without explicit alignment interaction a liquid-crystalline globule with nematic order can therefore only form in finite systems. The crossover becomes sharper for smaller systems because the entropic surface terms become more important compared to the isotropic interaction terms. The total value of the isotropic bulk interaction energy roughly scales as the volume of the globule, whilst the surface energy scales as the surface area of the globule. This shows that the transition to a liquid-crystalline polymer globule is actually driven by entropy, due to the entropic origin of the surface energy.

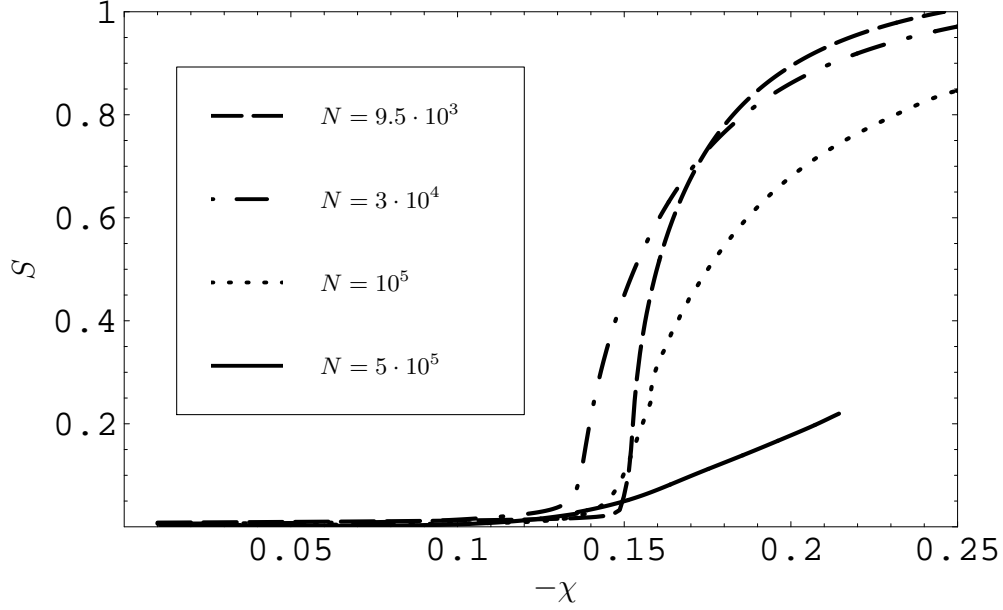


FIG. 15: The nematic order parameter  $S$  is plotted as a function of  $\chi$  for different chain lengths.

Finally, in Fig.(17), the average length  $L_R$  of the stiff parts is plotted as a function of  $\chi$  for  $N = 10^4$  and  $N = 5 \cdot 10^5$ . The figure shows that the average length of the rods is equal to 1 for very small values of  $\chi$  and  $\epsilon = 0$ . For  $N = 10^4$  it stays almost equal to 1 until the transition point is reached and then shows a rather strong increase. For very high values of  $\chi$  it should reach an asymptotic value. However, for  $\chi > 0.25$  the fraction of flexible segments ( $1 - \Theta_R$ , see Fig.(12)) becomes unphysically small indicating that the self-consistent field treatment reaches the limit of its validity. For  $N = 5 \cdot 10^5$  the crossover to a stronger increase in average rod length with  $-\chi$  is much smoother analogous to  $\Theta_R$  and  $S$  (see Figs.(14, 15)).

The stronger increase in average rod length for shorter polymers corresponding to a sharper isotropic-nematic transition indicates that this transition is also a cooperative process. To study the influence of cooperativity, the dependence of the isotropic-nematic transition on  $\sigma$  is discussed in the next subsection.

## 2. $\sigma$ -dependence

The crossover from amorphous globule to liquid-crystalline globule is a cooperative process. Fig.(18) shows that the crossover becomes sharper with increasing cooperativity (decreasing  $\sigma$ ) as expected. For very high cooperativity ( $\sigma = 10^{-5}$ ) and no selective interaction ( $\chi \approx 0$ ), the fraction of stiff segments ( $\Theta_R = 0.2$ ) is much smaller than  $1/2$ . When the transition point is approached, the fraction of stiff segments increases rapidly. For lower cooperativity (larger  $\sigma$ ), not only is the crossover much smoother but the fraction of stiff segments at  $\chi \approx 0$  is much higher ( $\Theta_R \approx 0.5$  for  $\sigma = 10^{-3}$  and  $\sigma = 5 \cdot 10^{-4}$ ). Both features clearly show the cooperativity of the transition.

The behavior of the nematic order parameter  $S$  for different values of  $\sigma$  is shown in Fig.(19). For higher  $\sigma$  the increase in nematic order is less steep and the transition point is significantly shifted to higher values of  $|\chi|$ . For  $\sigma = 5 \cdot 10^{-4}$  and higher, the system only develops a slight onset of order and  $S$  remains very small even deep in the globular state at  $\chi = -0.25$ . This again demonstrates the role of cooperativity in the formation of a liquid-crystalline globule.

It is therefore of interest to investigate the average rod length  $L_R$ , which should also strongly depend on the cooperativity. Fig.(20) shows that the increase of  $L_R$  with  $|\chi|$  after the transition point becomes steeper for smaller values of  $\sigma$  as one would expect. The isotropic-nematic transition is enhanced by cooperativity and even becomes impossible if the cooperativity is too small. As can be seen from Fig.(20), only a cooperative system forms long rods and not just many very short ones. Remember, that  $\sigma$  is associated with the energy penalty for a boundary between rod and coil, as discussed in the introduction. The smaller  $\sigma$  is, the larger is this energy penalty and the more favorable is the formation of long rods rather than short ones. It is intuitively clear that long rods align much easier



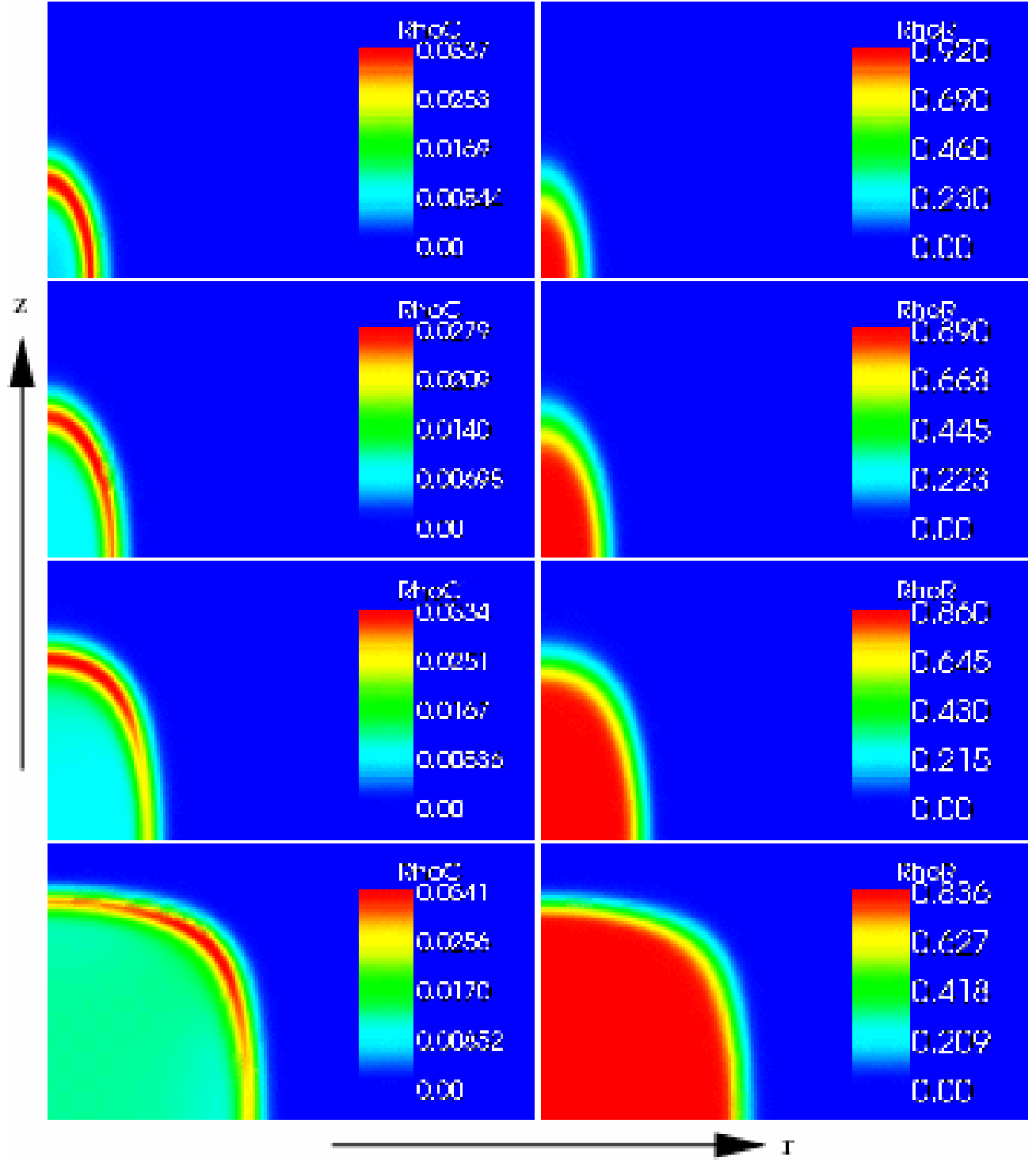


FIG. 16: The density of the flexible segments is shown on the left and the density of the stiff segments on the right.  $\sigma = 10^{-4}$ ,  $\epsilon = g = 0.0$  and  $\chi = -0.18$  for all plots. From top to bottom  $N$  increases as  $10^4$ ,  $3 \cdot 10^4$ ,  $10^5$  and  $5 \cdot 10^5$ .

than very short ones. When the average rod length stays roughly equal to 1 for high values of  $|\chi|$ , alignment cannot happen. Hence cooperativity is important to drive this transition.

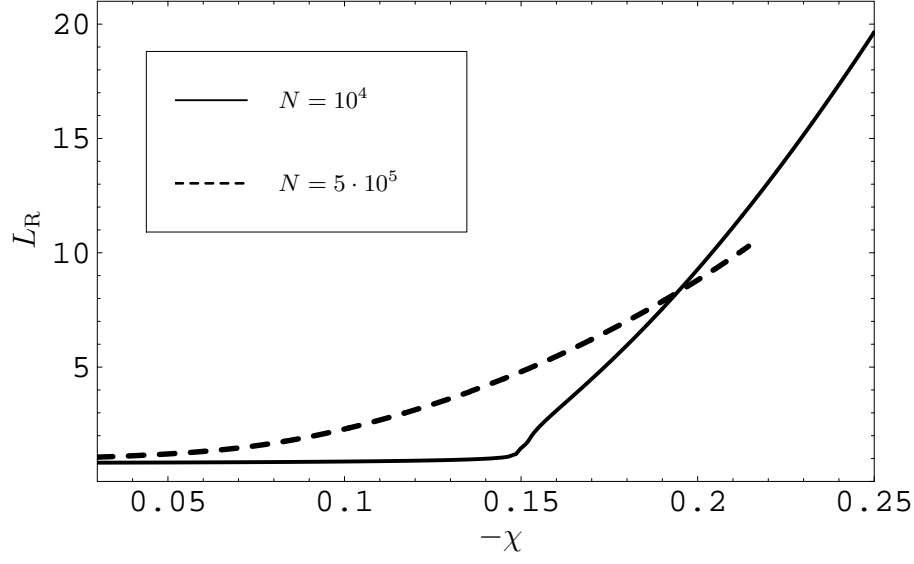


FIG. 17: The average length  $L_R$  of the stiff parts is plotted as a function of  $\chi$  for  $N = 10^4$  and  $N = 5 \cdot 10^5$ .

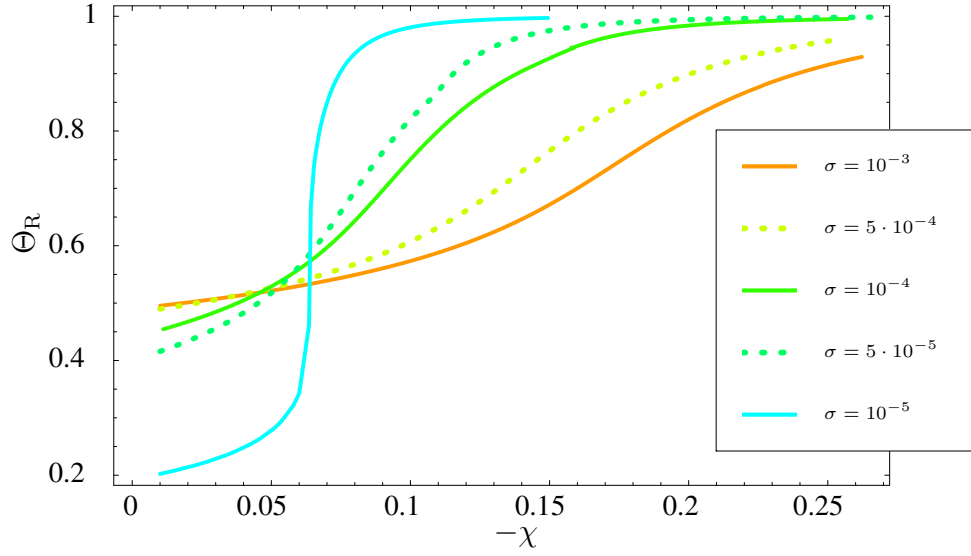


FIG. 18: The fraction of stiff segments is plotted as a function of  $\chi$  for different values of  $\sigma$  and  $N = 10^5$ ,  $\epsilon = g = 0$ . The crossover becomes sharper with decreasing  $\sigma$ , i.e. increasing cooperativity.

### 3. $\epsilon$ -dependence

In this subsection the  $\epsilon$ -dependence of the transition from amorphous to liquid-crystalline globule is investigated<sup>24</sup>. In Section IIB, it was shown that the fraction of stiff segments increases with increasing energy gain  $\epsilon$  per stiff segment. A higher value of  $\epsilon$  yields a higher offset of  $\Theta_R$  at  $\chi = 0$  which should in turn lead to a smaller value of  $|\chi|$  at the transition point.

Figs.(21, 22) demonstrate this behavior. For all plots in this subsection the cooperativity parameter is set to  $\sigma = 10^{-4}$  and the total chain length to  $N = 10^5$ . The explicit rod-rod alignment interaction is still switched off ( $g = 0$ ). The onset of the transition is indeed shifted to lower values of  $|\chi|$  with increasing energy gain per helical segments  $\epsilon$ . This is due to an increase of bulk interaction energy for fixed  $\chi$  with increasing number of stiff segments.

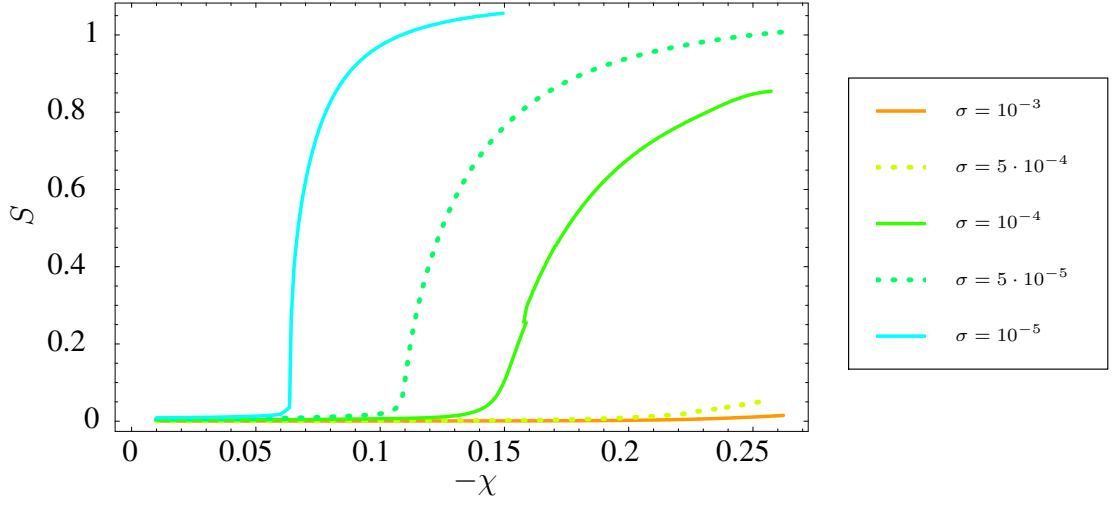


FIG. 19: The nematic order parameter  $S$  is plotted as a function of  $\chi$  for different values of  $\sigma$  and  $N = 10^5$ . The transition point is shifted to higher values of  $|\chi|$  with increasing  $\sigma$ .

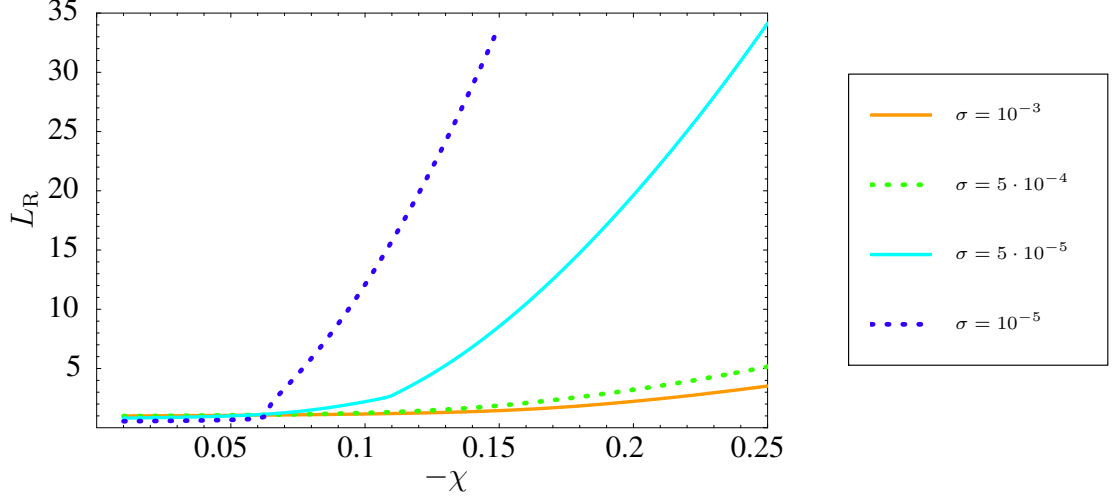


FIG. 20: The average rod length  $L_R$  is plotted as a function of  $\chi$  for different values of  $\sigma$  and  $N = 10^5$ .

The curves for  $\epsilon \geq 0.1$  in Figs.(21, 22) start at non-zero values of  $\chi$ . These values of  $\chi$  correspond to the transition point between open chain regime and globular regime, similar to the discussion in Section IIA. The main difference in this case is that at  $v = -0.2$  the non-selective attractive two-body interaction is not strong enough to drive the system into the globular state. The additional selective two-body interaction between the stiff segments only (with interaction parameter  $\chi$ ) is needed to drive the system into the globular state. That this is only the case for  $\epsilon \geq 0.1$  can be explained as follows (see also Section IIB). If there is no additional selective interaction energy which favors a compactification of the stiff segments, the stiffening of parts of the chain due to an increase of  $\Theta_R$  with increasing  $\epsilon$  pushes the chain segments further apart from each other and therefore leads to a more open structure. For  $\epsilon \geq 0.1$ , the system is thus pushed into the open chain regime at  $\chi = 0$ . On the other hand, for  $\epsilon \geq 0.17$  the system can be driven directly from open chain to liquid-crystalline globule as soon as  $|\chi|$  exceeds some crossover value.

These findings permit the computation of a complete phase diagram of the rod-coil copolymer in  $\epsilon$ - $\chi$  space, see Fig.(25). But before this is done, it has to be checked whether the definition of the transition point between coil and globule as the minimum of the  $N(\mu)$ -curve is also reasonable in the case of strong nematic order. In Section IIA the radius  $R$  of the globule (defined as the point at which the total density has decreased to  $\rho(R) = 10^{-3}\rho_0$ )

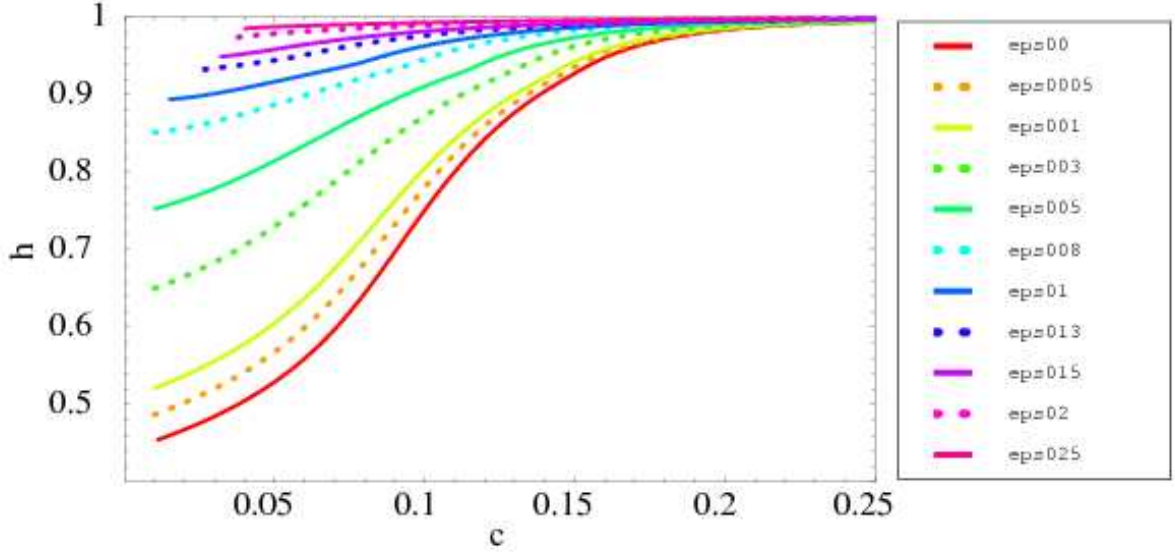


FIG. 21: Fraction of helical segments  $\Theta_R$  as a function of  $\chi$  for different values of the energy gain per helical segment  $\epsilon$ .

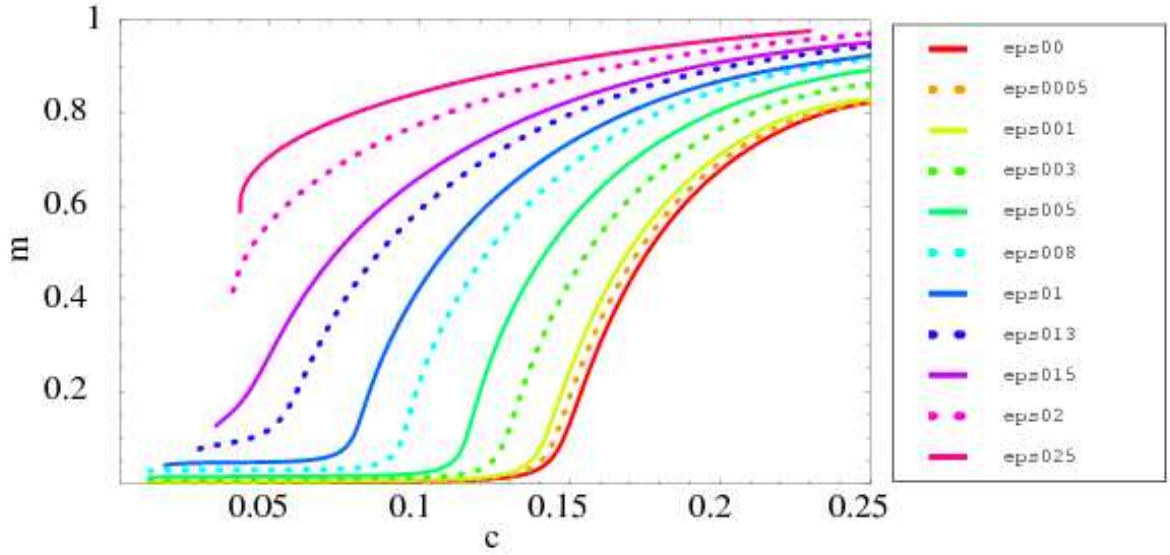


FIG. 22: Nematic order parameter  $S$  as a function of  $\chi$  for different values of  $\epsilon$ .

was plotted as a function of  $v$ , see Fig.(7). It showed a rapid increase when the transition point between globule and coil was approached. Here the globule shows nematic order and has an asymmetric shape, i.e. it is necessary to distinguish between  $\varrho$ - and  $z$ -direction. The extensions of the globule in  $\varrho$ -direction  $R_\varrho$  and in  $z$ -direction  $R_z$  are defined - analogously to  $R$  in the case of a spherical globule - as  $\rho(R_\varrho, 0) = \rho(0, R_z) = 10^{-3}\rho_0$ . In Fig.(23)  $R_\varrho$  and  $R_z$  are plotted as functions of  $\chi$  for  $\epsilon = 0.25$ . For this choice of  $\epsilon$ , the system already shows strong nematic order at  $\chi = -0.0396$  which corresponds to the transition point between globule and coil. Fig.(23) demonstrates that the definition of the transition point between open chain and globular regime as the minimum of the  $N$ - $\mu$  curve is valid even if the system shows strong nematic order. Both curves in Fig.(23) show a rapid increase when approaching the transition point from the right. The different values of  $R_\varrho$  and  $R_z$  reflect the cylindrical shape of the globule due to the nematic order of the stiff segments. For  $\epsilon = 0.25$  no isotropic globular phase exists and the crossover leads directly to a liquid-crystalline globule.

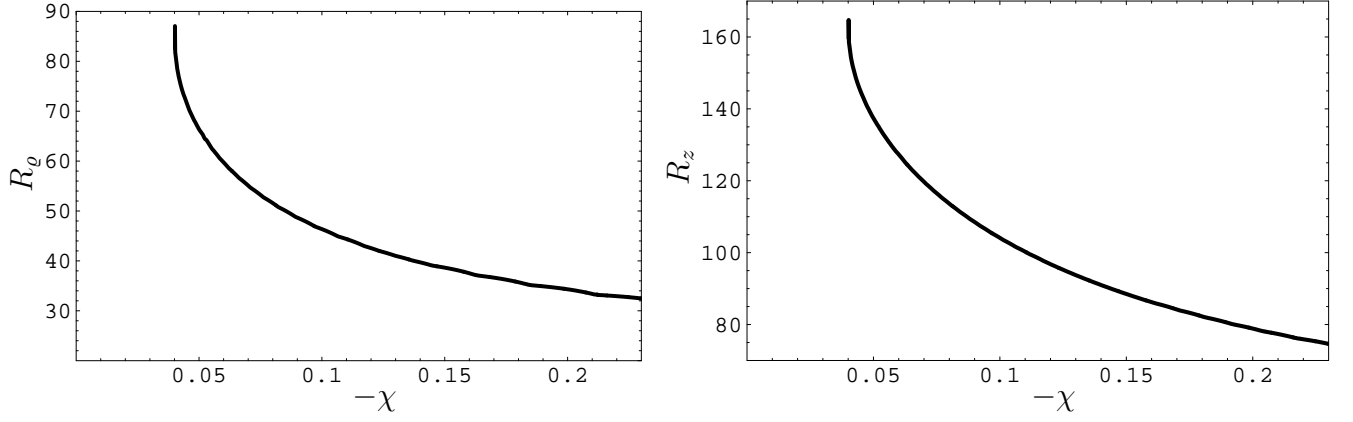


FIG. 23: The extensions of the globule in  $\rho$ -direction  $R_\rho$  and in  $z$ -direction  $R_z$  are plotted as functions of  $\chi$  for  $\epsilon = 0.25$ .

For  $\epsilon = 0.1$  on the other hand, the system shows no nematic order at the transition point between open chain and globule ( $\chi = -0.0138$ ). The system therefore undergoes two transitions. First from an open chain to an amorphous globule and then at higher  $|\chi|$  from an amorphous to a liquid-crystalline globule. In Fig.(24)  $R_\rho$  and  $R_z$  are plotted as functions of  $\chi$ . When the transition point between open chain and globule (at  $\chi = -0.0138$ ) is approached from

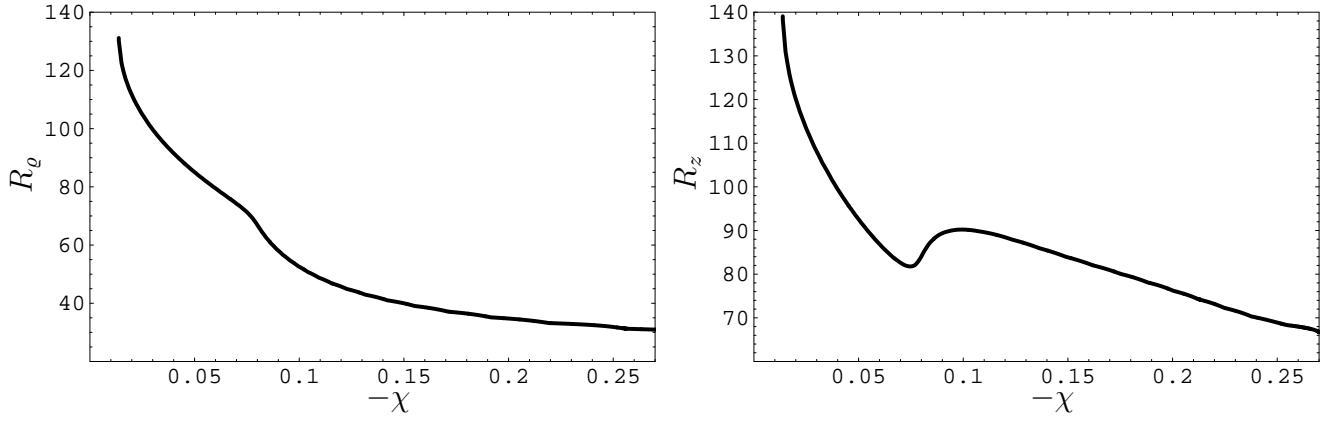


FIG. 24: The extensions of the globule in  $\rho$ -direction  $R_\rho$  and in  $z$ -direction  $R_z$  are plotted as functions of  $\chi$  for  $\epsilon = 0.1$ .

the right,  $R_\rho$  and  $R_z$  show the expected strong increase. When the transition point between amorphous and liquid-crystalline globule (at  $\chi = -0.0812$ ) is approached from the left,  $R_\rho$  and  $R_z$  show a different behavior. In a small interval (corresponding to the width of the transition)  $R_z$  increases whilst  $R_\rho$  decreases even stronger than before. In this interval the asymmetric shape of the globule is developed. This behavior will be discussed further in Subsection D.

As already mentioned above, it is now possible to compute a complete phase diagram in  $\epsilon$ - $\chi$  space. This phase diagram is shown in Fig.(25). The triangles are the transition points between open chain and globule. The squares are the transition points between amorphous and liquid-crystalline globule. Note, that the points plotted in the phase diagram, Fig.(25), are what is defined above as the points of rather broad crossover regions. Therefore the boundaries in the phase diagram have to be understood as center lines of broader regions in which the crossover from one phase to the other occurs. The little arrows in Fig.(25) correspond each to one of the rows of the color coded density plots shown in Fig.(13), helping to illustrate how the density profiles look at these points in the phase diagram.

#### 4. $g$ -dependence

The transition from amorphous to liquid-crystalline globule occurs without an explicit angle-dependent alignment interaction between the rods. It is nevertheless interesting to switch the explicit rod-rod alignment interaction on

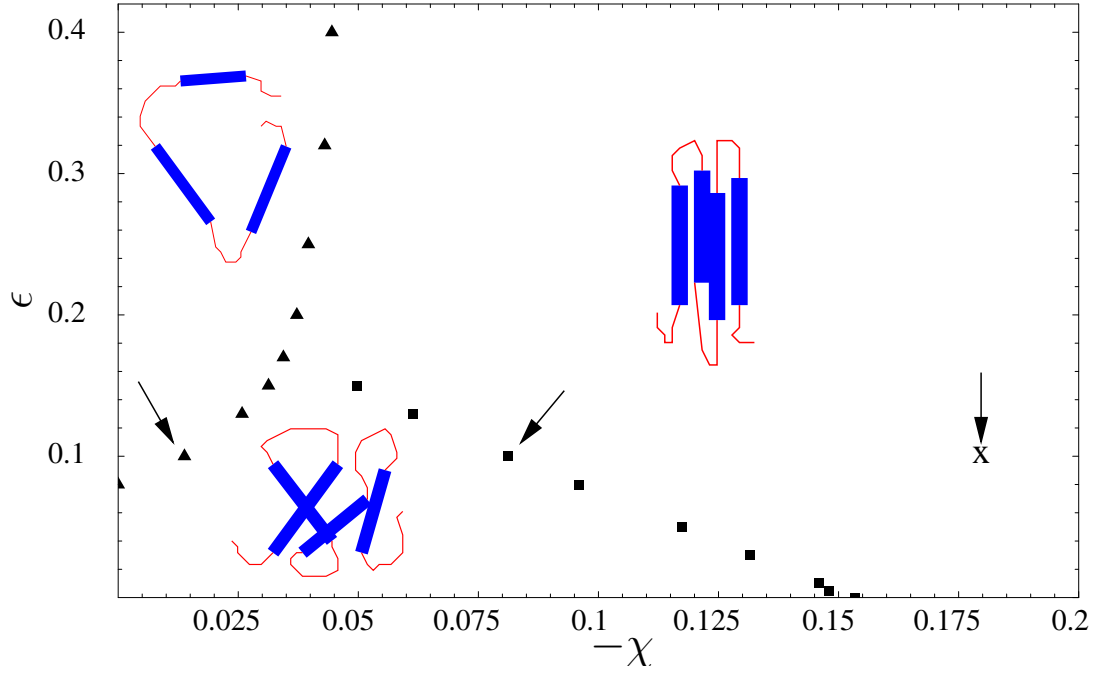


FIG. 25: Phase diagram of a rod-coil copolymer in  $\epsilon$ - $\chi$  space. The upper left area corresponds to an open chain, the lower left area to an amorphous globule and the right area to a nematic liquid-crystalline-globule. The little arrow to the left indicates the point in the phase diagram which corresponds to the top two pictures in Fig.(13). The arrow in the middle corresponds to the middle two pictures and the arrow to the right to the bottom ones. Parameters:  $N = 10^5$ ,  $\sigma = 10^{-4}$ ,  $g = 0$ .

and study its influence on the transition. The alignment interaction is of the Maier-Saupe form and its strength is controlled by the interaction parameter  $g$ , see Eq.(2.20). It is chosen to be attractive to favor alignment of the rods.

In Fig.(26) the fraction of stiff segments is plotted as a function of  $\chi$  for different values of  $g$  and  $\sigma = 10^{-4}$ ,  $\epsilon = 0$ ,  $N = 9.5 \cdot 10^3$ . The corresponding nematic order parameter  $S$  is shown in Fig.(27). The transition is shifted to

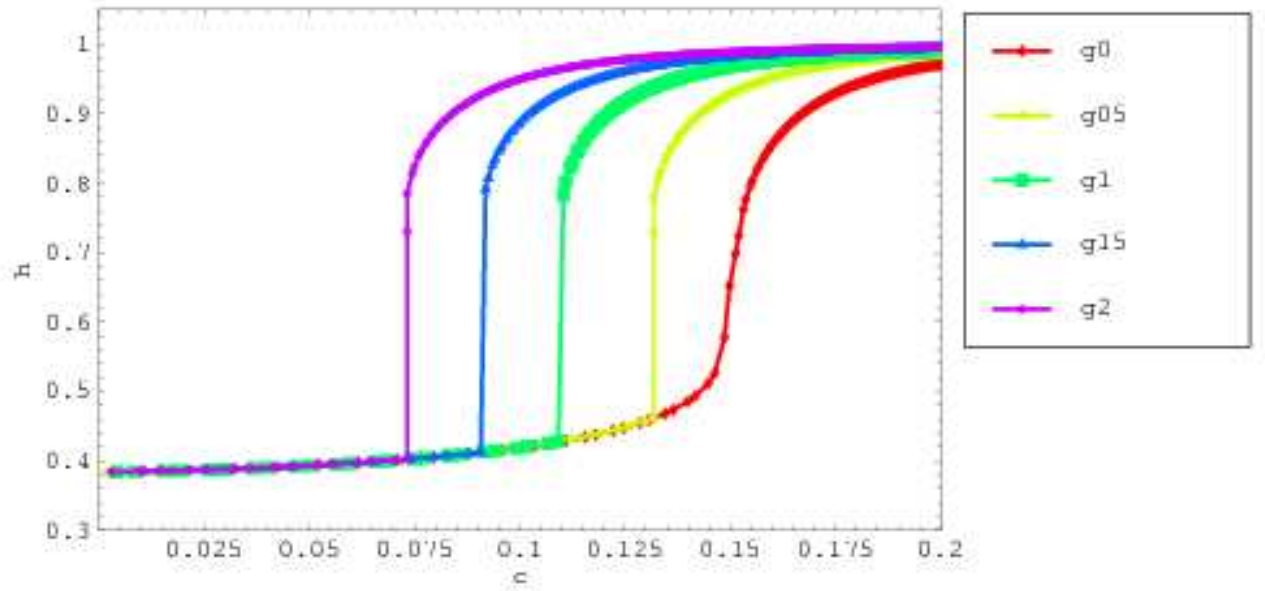


FIG. 26: Fraction of helical segments  $\Theta_R$  as a function of  $\chi$  for different values of  $g$ .

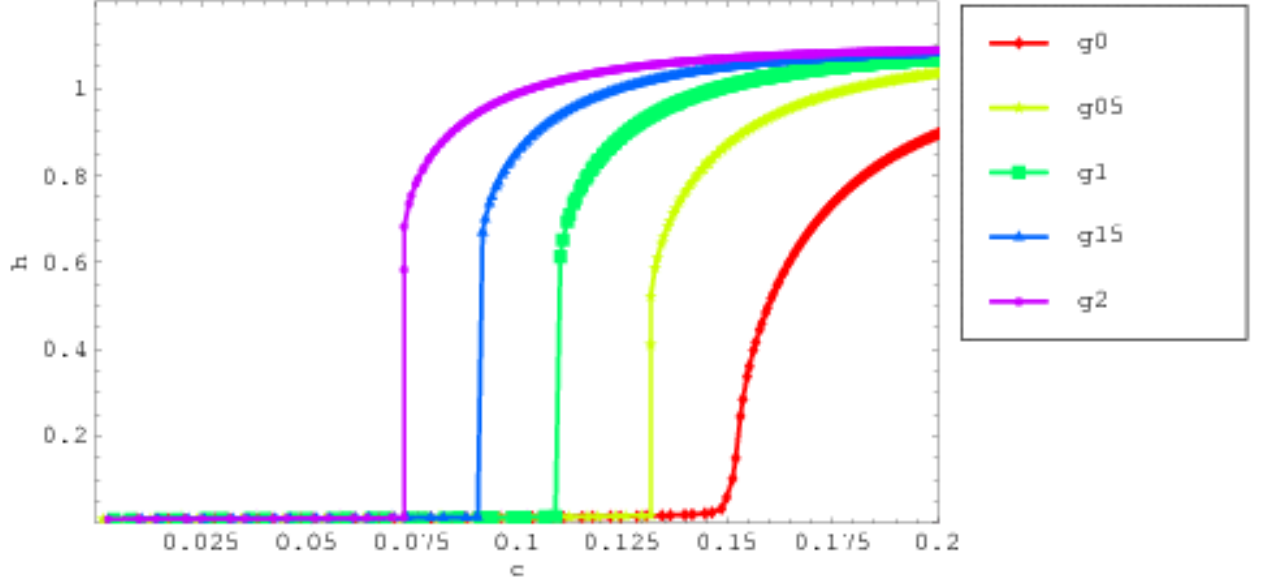


FIG. 27: Nematic order parameter  $S$  as a function of  $\chi$  for different values of  $g$ .

lower values of values of  $|\chi|$  with increasing  $|g|$ . This is not surprising, since for  $g < 0$  the alignment term provides an additional incentive for the system to generate nematic order and stiff segments. But the fact that almost up to the respective transition points the  $\Theta_R(\chi)$ -curves lie perfectly on top of each other is quite remarkable. This can be explained as follows. For  $\psi_2 \equiv 0$  the alignment term in Eq.(2.20) is equal to zero. Therefore the system has to generate a finite  $\psi_2$  (i.e. at least small nematic order) before the alignment interaction can have an effect on the system. As long as there is no nematic order in the system ( $\psi_2 \equiv 0$ ) the alignment term is zero and the system behaves as the one with  $g = 0$ . As expected, the attractive alignment interaction enhances the generation of nematic order and thus shifts the transition point to lower values of  $|\chi|$ .

#### D. Free energy

In this subsection the behavior of the effective free energy in the crossover region is investigated. The effective saddle point grand potential  $\Omega$  is given by Eq.(2.20). With the definition of the chemical potential used here the corresponding effective saddle point free energy is given by

$$F = \Omega - \mu N. \quad (3.4)$$

In Fig.(28) the free energy  $F$  is plotted as a function of  $\chi$  for  $\sigma = 10^{-4}$ ,  $N = 9.5 \cdot 10^3$  and  $\epsilon = g = 0$ . These parameters are the same as the ones used in Fig.(12). Fig.(28) demonstrates that the free energy is changing its slope in the crossover region around the transition point as would be expected for a crossover. At the beginning of Section IIC the occurrence of the transition from amorphous to liquid-crystalline globule was explained in terms of the interplay between surface energy and bulk interaction energy. Because of the anisotropy of the surface contributions which originate from the entropy of the rods, the globule tries to minimise its surface in  $z$ -direction and to maximise it in  $\varrho$ -direction. Before the transition the amorphous globule has a spherical shape. The surface energies in  $x$ -,  $y$ - and  $z$ -direction should therefore be all the same. For the cylindrical coordinates used here that implies  $F_\varrho^{\text{surf}} = 2F_z^{\text{surf}}$ . Fig.(29) shows that this is indeed the case. But also in the liquid-crystalline globule regime after the transition their ratio is roughly equal to 2 as can be seen from Fig.(29). The extension of the globule in  $\varrho$ - and  $z$ -direction on the other hand is now very different. It is therefore instructive to plot  $F_\varrho^{\text{surf}}$  and  $F_z^{\text{surf}}$  normalized by the corresponding cross sections of the globule, which should give a feeling how the surface tension behaves. As an approximation of the cross section in  $z$ -direction  $R_\varrho^2$  is chosen. The cross section in  $\varrho$ -direction is approximated by  $R_\varrho R_z$ , where  $R_\varrho$  and  $R_z$  are defined as in Subsection IIC3. In Fig.(30) the normalized surface contributions are plotted on the left hand side and  $R_\varrho$  and  $R_z$  on the right hand side. The plot on the left shows that the surface energy per area in  $z$ -direction becomes indeed larger than the one in  $\varrho$ -direction in the interval in which the crossover from amorphous

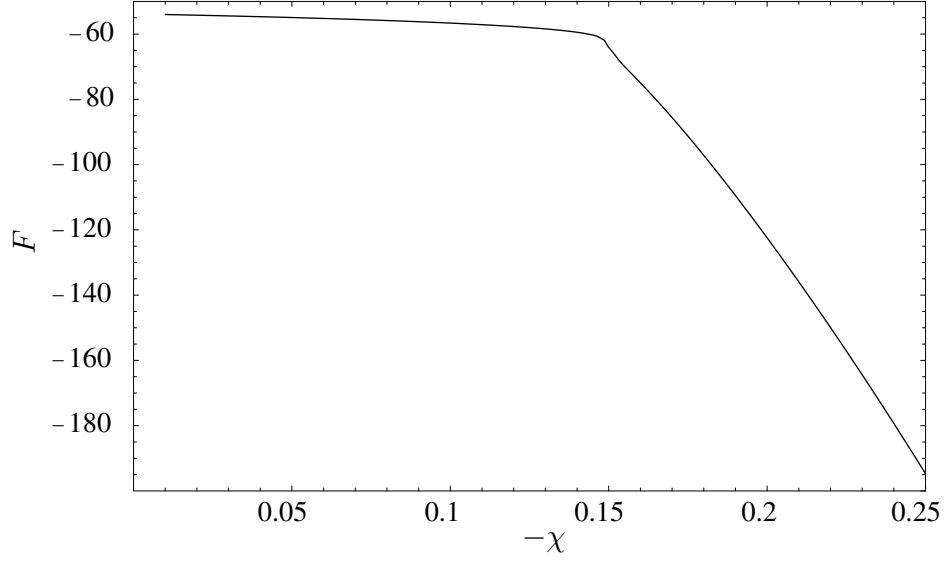


FIG. 28: Free energy  $F$  plotted as a function of  $\chi$  for  $\sigma = 10^{-4}$ ,  $N = 9.5 \cdot 10^3$  and  $\epsilon = g = 0$ .

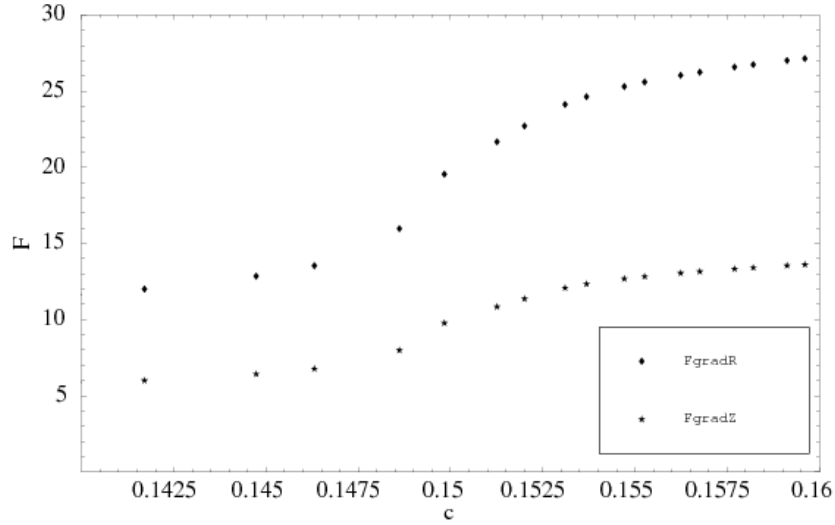


FIG. 29:  $F_{\rho}^{\text{surf}}$  and  $F_z^{\text{surf}}$  plotted as functions of  $\chi$  for  $\sigma = 10^{-4}$ ,  $N = 9.5 \cdot 10^3$  and  $\epsilon = g = 0$ .

globule to liquid-crystalline globule occurs. The corresponding extensions of the globule  $R_{\rho}$  and  $R_z$  plotted on the right illustrate the enlargement of the globule in  $z$ -direction and the diminution in  $\rho$ -direction in the crossover interval. When the final shape of the liquid-crystalline globule has developed the curves become parallel again and decrease both indicating the further compactification of the entire globule. The investigations of the surface contributions to the free energy further visualize that it is the anisotropy of the entropic surface energy that drives the system into the nematic state.

#### IV. CONCLUSIONS

The numerical solutions of the self-consistent field equations show that the rod-coil copolymer with variable composition can form three phase states, open chain, amorphous globule and nematic liquid-crystalline globule with high



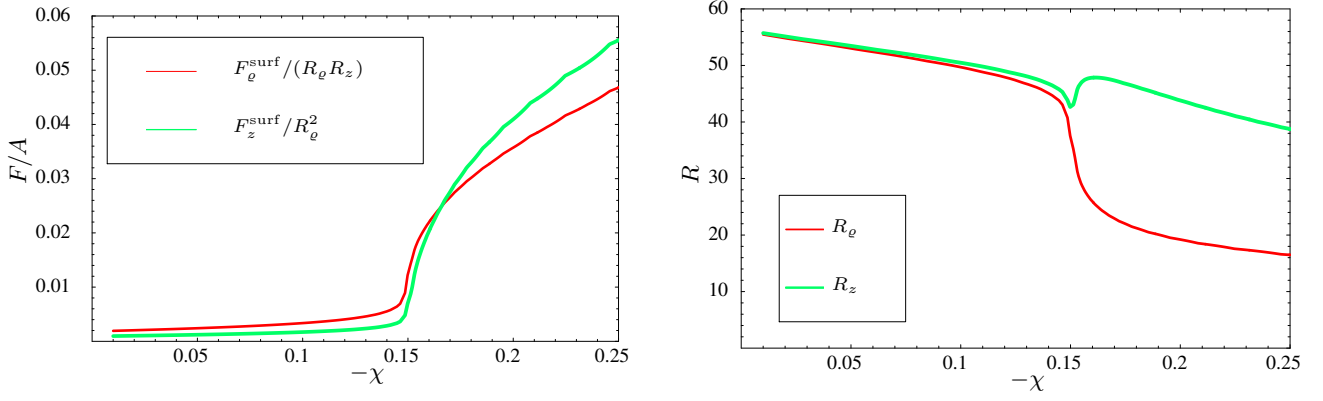


FIG. 30:  $F_e^{\text{surf}}/(R_e R_z)$  and  $F_z^{\text{surf}}/(R_e^2)$  plotted as functions of  $\chi$  for  $\sigma = 10^{-4}$ ,  $N = 9.5 \cdot 10^3$  and  $\epsilon = g = 0$ .

fraction of stiff segments. The transition between the first two states is similar to the coil-globule transition of a homopolymer. The formation of a liquid-crystalline globular state without explicit alignment interaction between the rods is a novel result and deserves further discussion.

The formation of a liquid-crystalline globule from a rod-coil multiblock copolymer with fixed composition has been discussed for the first time in an early theoretical work<sup>27</sup>. Phase states similar to the ones summarized in the phase diagram in Fig.(25) have been seen in<sup>28</sup>, where the authors consider a homopolymer in which each monomer carries a dipole moment and take into account explicit dipole-dipole interactions. However, the schematic phase diagram in<sup>28</sup> has been considered within the so-called volume approximation where the contribution of the surface energy can be neglected (at  $N \rightarrow \infty$ )<sup>22</sup> and the transition into the anisotropic globular state with nematic order is driven by dipole-dipole interactions.

Recently, in the paper by Marenduzzo et al.<sup>29</sup> a new class of models for chain molecules has been considered. This model can be viewed as an elastic tube and the concept of the chain thickness ("thick polymer") has been introduced by means of a specially prescribed three-body interaction potential. Nevertheless, we should stress that on the mean-field level the consideration (within the so-called "chain of coins" model) is still limited to the *volume approximation*, and the explicit alignment interaction in form of an Onsager second virial term is present (see the Eq.(14) in ref. <sup>29</sup>). In contrast to this in our case the formation of a LC-globule occurs without explicit alignment interactions between the helical parts. It is the entropic surface tension anisotropy which drives the globule in the nematic LC-state.

In an early work<sup>30</sup> a cooperative helix-coil liquid-crystal transition has been found, very similar to the transition from amorphous to liquid-crystalline globule discussed here. The formation of nematic order is also accompanied by a strong increase in fraction of stiff (or helical) segments. The main difference is again that the transition is driven by an explicit alignment interaction of Maier-Saupe type similar to the additional interaction ( $g < 0$ ) considered in Section IIC4 and not by the entropic surface tension anisotropy.

Monte Carlo simulations of a simple homopolymer model on the lattice have been carried out to study the interplay between coil-globule transition and  $\alpha$ -helix formation<sup>14</sup>. The phase diagram has been presented in terms of two energetic parameters that characterize the hydrophobic attraction between monomers that are far apart in sequence and the local helix-stabilizing interaction. This is reminiscent of our  $\chi - \epsilon$  diagram given in Fig.25. The number of helical units,  $\langle \Xi \rangle$ , (helicity) and the number of pairwise contacts,  $\langle NC \rangle$ , are used as criteria to distinguish among different phases. Following these criteria the authors are able to see four different phases. Nevertheless it is difficult to compare these results with our findings because the order parameters we use are substantially different from the ones used in ref.<sup>14</sup>.

In the context of secondary and tertiary structure formation in proteins the interplay of helix formation and liquid-crystalline order has been studied, see for instance<sup>31,32</sup>. It was shown that liquid-crystalline ordering enhances the number of helical segments as well as the average length of the helices which is qualitatively similar to the results of the model presented here. This indicates that the model of a rod-coil multiblock copolymer with variable composition might be a good candidate to give a simple explanation for the formation of helix bundles in certain globular proteins. Both, simulations<sup>33</sup> and experiments<sup>34</sup> show that proteins can adopt not only the native and completely denatured state (open chain) but also so-called premolten and molten globular states. For helix-bundle proteins the premolten globule, which does not show any order of the helices, corresponds to the amorphous globule in our model. The molten globule with ordered helices but without native contacts (and therefore also without the characteristic helix-helix angle found in the native state) corresponds to the liquid-crystalline globule. Our model also shows that during the transition

to a liquid-crystalline globule not only the amount of helical segments increases strongly but the globule also becomes more compact. The experimentally observed<sup>11</sup> correlation between the amount of secondary structure elements and compactness of proteins mentioned in the introduction might therefore also be explained by this transition, at least in the case of helix bundle proteins.

Irrespective of the possible application to helix bundle formation in proteins, the model which we have discussed in this paper provides a relatively simple example of the general interplay between secondary structure (helices or stiff rods) and tertiary structure (liquid-crystalline order) in homopolypeptides.

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